جمهورية العراق وزارة التعليم العالي جامعة تكريت كليةالهندسةالشرقاط قسم الهندسة ميكانيك



Thermodynamics Lecture 2<sup>nd</sup> class

BY



2021/2022



دكتواره في الهندسة الميكانيكيه

Email: abdulrazzaq.saleh@tu.edu.iq

**Thermodynamics** can be defined as the science of *energy*. The name *thermodynamics* stems from the Greek words *therme* (heat) and *dynamis* (power)

**Energy** can be viewed as the ability to cause changes.

One of the most fundamental laws of nature is the *Conservation of energy principle*. It simply states that during an interaction, energy can change from one form to another but the total amount of energy remains constant. That is, energy cannot be created or destroyed.

A rock falling off a cliff, for example, picks up speed as a result of its potential energy being converted to kinetic energy (Fig. 1–1).

The **First law of thermodynamics** is simply an expression of the conservation of energy principle, and it asserts that *energy* is a thermodynamic property.

A person who has a greater energy input (food) than energy output (exercise) will gain weight (store energy in the form of fat), and a person who has a smaller energy input than output will lose weight (Fig. 1–2).

The **Second law of thermodynamics** asserts that energy has *quality* as well as *quantity*, and actual processes occur in the direction of decreasing quality of energy.

For example, a cup of hot coffee left on a table eventually cools, but a cup of cool coffee in the same room never gets hot by itself (Fig. 1–3).





# FIGURE 1–1

Energy cannot be created or destroyed; it can only change forms (the first law)





Conservation of energy principle for the human body

FIGURE 1–3 Heat flows in the direction of decreasing temperature.

This macroscopic approach to the study of thermodynamics that does not require a knowledge of the behavior of individual particles is called *classical thermodynamics*. It provides a direct and easy way to the solution of engineering problems.

A more elaborate approach, based on the average behavior of large groups of individual particles, is called *statistical thermodynamics*. This microscopic approach is rather involved and is used in this text only in the supporting role.

# 1.1 Application Areas of Thermodynamics

Thermodynamics is commonly encountered in many engineering systems and other aspects of life, and one does not need to go very far to see some application areas of it. In fact, one does not need to go anywhere. The heart is constantly pumping blood to all parts of the human body, various energy conversions occur in trillions of body cells, and the body heat generated is constantly rejected to the environment. The human comfort is closely tied to the rate of this metabolic heat rejection. We try to control this heat transfer rate by adjusting our clothing to the environmental conditions. Other applications of thermodynamics are right where one lives. An ordinary house is, in some respects, an exhibition hall filled with wonders of thermodynamics (Fig. 1-4).



#### FIGURE 1–4



# **1.2 IMPORTANCE OF DIMENSIONS AND UNITS**

Any physical quantity can be characterized by *dimensions*. The magnitudes assigned to the dimensions are *called units*. Some basic dimensions such as mass *m*, length *L*, time *t*, and temperature *T* are selected as *primary* or *fundamental dimensions*, while others such as velocity *V*, energy *E*, and volume *V* are expressed in terms of the primary dimensions and are called *secondary dimensions*, or *derived dimensions*. A number of unit systems have been developed over the years. Despite strong efforts in the scientific and engineering community to unify the world with a single unit system, two sets of units are still in common use today: The *English system*, which is also known as the *United States*.



Refrigerator © McGraw-Hill Education, Jill Braaten



Power plants © Malcolm Fife/Getty Images RF



Wind turbines © F. Schussler/PhotoLink/Getty Images RF

FIGURE 1-5

Some application areas of thermodynamics

# **1.3 Some SI and English Units**

As pointed out, the SI is based on a decimal relationship between units. The prefixes used to express the multiples of the various units are listed in **Table 1–2**. They are standard for all units, and the student is encouraged to memorize them because of their widespread use (Fig. 1–6).

1 Ibm = 0.45359 kg

1 ft = 0.3048 m



© Doug Menuez/Getty Images RF



Human body © Ryan McVay/Getty Images RF



Food processing Glow Images RF



Aircraft and spacecraft © PhotoLink/Getty Images RF



Cars © Mark Evans/Getty Images RF



A piping network in an industrial facility. Courtesy of UMDE Engineering Contracting and Trading. Used by permission



**FIGURE 1–6** The SI unit prefixes are used in all branches of engineering.

In SI, the force unit is the **newton** (N), and it is defined as the *force required to accelerate a mass of 1 kg at a rate of 1 m/s2*. In the English system, the force unit is the **pound-force** (lbf) and is defined as the *force required to accelerate a mass of 32.174 lbm (1 slug) at a rate of 1 ft/s2* (Fig. 1–7).

> F = (Mass) (acceleration) F = m × a 1 N = 1 Kg . m /s<sup>2</sup> 1 Ibf = 32.174 Ibm . ft/s<sup>2</sup>



**FIGURE 1–7** The definition of the force units.

A force of 1 N is roughly equivalent to the weight of a small apple (m = 102 g), whereas a force of 1 lbf is roughly equivalent to the weight of our medium apples (mtotal = 454 g) as shown in Fig. 1–8. Another force unit in common use in many European countries is the *kilogram-force* (kgf), which is the weight of 1 kg mass at sea level (1 kgf = 9.807 N).



# TABLE 1-1

The seven fundamental (or primary) dimensions and their units in SI

Dimension	Unit
Length	meter (m)
Mass	kilogram (kg)
Time	second (s)
Temperature	kelvin (K)
Electric current	ampere (A)
Amount of light	candela (cd)
Amount of matter	mole (mol)

# TABLE 1-2

Standard prefixes in SI units					
Multiple	Prefix				
1024	yotta, Y				
10 <sup>21</sup>	zetta, Z				
10 <sup>18</sup>	exa, E				
10 <sup>15</sup>	peta, P				
1012	tera, T				
10 <sup>9</sup>	giga, G				
10 <sup>6</sup>	mega, M				
10 <sup>3</sup>	kilo, k				
10 <sup>2</sup>	hecto, h				
10 <sup>1</sup>	deka, da				
10 <sup>-1</sup>	deci, d				
10-2	centi, c				
10 <sup>-3</sup>	milli, m				
10 <sup>-6</sup>	micro, μ				
10 <sup>-9</sup>	nano, n				
10 <sup>-12</sup>	pico, p				
10 <sup>-15</sup>	femto, f				
10 <sup>-18</sup>	atto, a				
10-21	zepto, z				
10-24	yocto, y				

The term *weight* is often incorrectly used to express mass, particularly by the "weight watchers." Unlike mass, weight W is a *force*. It is the gravitational force applied to a body, and its magnitude is determined from Newton's second law,

#### W = m g(N)

A body weighs less on top of a mountain since g decreases with altitude. On the surface of the moon, an astronaut weighs about one sixth of what she or he normally weighs on earth (Fig. 1–9).

At sea level a mass of 1 kg weighs 9.807 N, as illustrated in Fig. 1-10. A mass of 1 lbm, however, weighs 1 lbf, which misleads people to believe that pound-mass and pound-force can be used interchangeably as pound (lb), which is a major source of error in the English system.

*Work*, which is a form of energy, can simply be defined as force times distance; therefore, it has the unit A body weighing 150 lbf on earth will weigh "newton-meter  $(N \cdot m)$ ," which is called a **joule** (J). That N·m is,

$$1 J = 1 N \cdot m$$
$$1 KJ = 10^3 J$$

In the English system, the energy unit is the **Btu** (British thermal unit), which is defined as the energy required to raise the temperature of 1 lbm of water at 68°F by 1°F. In the metric system, the amount of energy needed to raise the temperature of 1 g of water at 14.5°C by 1°C is defined as 1 calorie (cal),

# 1 cal = 4.1868 J.1 Btu = 1.0551 kJ

The unit for time rate of energy is joule per second (J/s), which is called a *watt* (W).



#### FIGURE 1–9

only 25 lbf on the moon.



#### **FIGURE 1–10**

The weight of a unit mass at sea level.



**FIGURE 1–11** Always check the units in your calculations

# **1.5 SYSTEMS AND CONTROL VOLUMES**

A system is defined as a quantity of matter or a region in space chosen for study. The mass or region outside the system is called the **surroundings**. The real or imaginary surface that separates the system from its surroundings is called the **boundary (Fig. 1–12).** The boundary of a system can be fixed or movable. Note that the boundary is the contact surface shared by both the system and the surroundings. Mathematically speaking, the boundary has zero thickness, and thus it can neither contain any mass nor occupy any volume in space. Systems may be considered to be closed or open, depending on whether a fixed mass or a fixed volume in space is chosen for study. A **closed system** (also known as a **control mass** or just system when the context makes it clear) consists of a fixed amount of mass, and no mass can cross its boundary. That is, no mass can enter or leave a closed system, as shown in *Fig. 1–13*. But energy, in the form of heat or work, can cross the boundary; and the volume of a closed system does not have to be fixed. If, as a special case, even energy is not allowed to cross the boundary, that system is called an *isolated system*.

Consider the piston-cylinder device shown in **Fig. 1–14.** Let us say that we would like to find out what happens to the enclosed gas when it is heated. Since we are focusing our attention on the gas, it is our system. The inner surfaces of the piston and the cylinder form the boundary, and since no mass is crossing this boundary, it is a closed system. Notice that energy may cross the boundary, and part of the boundary (the inner surface of the piston, in this case) may move. Everything outside the gas, including the piston and the cylinder, is the surroundings.



An *open system*, or a *control volume*, as it is often called, is a properly selected region in space. It usually encloses a device that involves mass flow such as a compressor, turbine, or nozzle. Flow through these devices is best studied by selecting the region within the device as the control volume. Both mass and energy can cross the boundary of a control volume.

In the case of a nozzle, the inner surface of the nozzle forms the real part of the boundary, and the entrance and exit areas form the imaginary part, since there are no physical surfaces there (Fig. 1-15a).

control volume can be fixed in size and shape, as in the case of a nozzle, or it may involve a moving boundary, as shown in Fig. 1–15b. As an example of an open system, consider the water heater shown in Fig. 1–16.





(a) A control volume (CV) with real and imaginary boundaries



(b) A control volume (CV) with fixed and moving boundaries as well as real and imaginary boundaries

# FIGURE 1–15

A control volume can involve fixed, moving, real, and imaginary boundaries.

FIGURE 1–16 An open system (a control volume) with one inlet and one exit.

# **1.6 PROPERTIES OF A SYSTEM**

Any characteristic of a system is called a *property*. Some familiar properties are pressure *P*, temperature *T*, volume *V*, and mass *m*. The list can be extended to include less familiar ones such as viscosity, thermal conductivity, modulus of elasticity, thermal expansion coefficient, electric resistivity, and even velocity and elevation

Properties are considered to be either intensive or extensive. Intensive properties are those that are independent of the mass of a system, such as temperature, pressure, and density. Extensive properties are those whose values depend on the size or extent of the system.as shown in Fig. 1–17. Extensive properties per unit mass are called **specific** properties. Some examples of specific properties are specific volume (v = V/m) and specific total energy (e = E/m).



Extensive properties

Intensive properties

# FIGURE1–17 Criterion to differentiate intensive and extensive properties.

# **1.6 STATE AND EQUILIBRIUM**

Thermodynamics deals with equilibrium states.

The word *equilibrium* implies a state of balance. In an equilibrium state there are no unbalanced potentials (or driving forces) within the system.

thermal equilibrium if the temperature is the same throughout the entire system, as shown in *Fig.* 1–18.

Mechanical equilibrium is related to pressure, and a system is in mechanical equilibrium if there is no change in pressure at any point of the system with time

If a system involves **two** phases, it is in **phase** equilibrium when the mass of each phase reaches an equilibrium level and stays there

chemical equilibrium if its chemical composition does not change with time, that is, no chemical reactions occur.



(a) Before

**FIGURE 1–18** 

A closed system reaching thermal equilibrium.

#### **1.7 PROCESSES AND CYCLES**

Any change that a system undergoes from one equilibrium state to another is called a **process**, and the series of states through which a system passes during a process is called the **path** of the process (*Fig. 1–19*). When a process proceeds in such a manner that the system remains infinitesimally close to an equilibrium state at all times, it is called a **quasi-static**, or **quasi-equilibrium**, **process**.



diagram of a compression process of a gas.

An *isothermal process*, for example, is a process during which the temperature T remains constant; an *isobaric process* is a process during which the pressure P remains constant; and an *isochoric (or isometric) process* is a process during which the specific volume v remains constant.

A system is said to have undergone a *cycle* if it returns to its initial state at the end of the process. That is, for a cycle the initial and final states are identical.



(1)

 $V_2$ 

(2)

System

#### **1.8 The Steady-Flow Process**

The terms steady and uniform are used frequently in engineering, and thus it is important to have a clear understanding of their meanings. The term **steady** implies no change with time. The opposite of steady is **unsteady**, *or* **transient**. The term **uniform**, however, implies no change with location *over* a specified region. These meanings are consistent with their everyday use (steady girlfriend, uniform properties, etc.)

large number of engineering devices operate for long periods of time under the same conditions, and they are classified as *steadyflow devices* 

*steady-flow process*, which can be defined as a process during which a fluid flows through a control volume steadily (Fig. 1–22). That is, the fluid properties can change from point to point within the control volume, but at any fixed point they remain the same during the entire process. Therefore, the volume V, the mass m, and the total energy content E of the control volume remain constant during a steady flow process (Fig. 1–23).

Steady-flow conditions can be closely approximated by devices that are intended for continuous operation such as turbines, pumps, boilers, condensers, and heat exchangers or power plants or refrigeration systems.



#### FIGURE 1–24

Two bodies reaching thermal equilibrium after being brought into contact in an isolated enclosure.



**FGURE1–22** During a steady-flow process, fluid properties within the control volume may change with position but not with time.



**FIGURE 1–23** Under steady-flow conditions, the mass and energy contents of a control volume remain constant

That is, when a body is brought into contact with another body that is at a different temperature, heat is transferred from the body at higher temperature to the one at lower temperature until both bodies attain the same temperature (Fig. 1-24).

At that point, the heat transfer stops, and the two bodies are said to have reached **thermal** equilibrium

# **1.8 TEMPERATURE AND THE ZEROTH LAW OF THERMODYNAMICS**

The **zeroth law of thermodynamics** states that if two bodies are in thermal equilibrium with a third body, they are also in thermal equilibrium with each other.

By replacing the third body with a thermometer, *the zeroth law can be restated as* two bodies are in thermal equilibrium if both have the same temperature reading even if they are not in contact

# **1.8 Temperature Scales**

All temperature scales are based on some easily reproducible states such as the freezing and boiling points of water, which are also called the *ice point* and the *steam point*, respectively. A mixture of ice and water that is in equilibrium with air saturated with vapor at 1 atm pressure is said to be at the **ice point** and a mixture of liquid water and water vapor (with no air) in equilibrium at 1 atm pressure is said to be at the **steam point**.

The temperature scales used in the SI and in the English system today are the *Celsius scale and* the *Fahrenheit scale in English unit system* 

In thermodynamics, it is very desirable to have a temperature scale that is independent of the properties of any substance or substances. Such a temperature scale is called a *thermodynamic temperature scale* 

The thermodynamic temperature scale in the SI is the Kelvin scale

The thermodynamic temperature scale in the English system is the *Rankine scale* 

temperature scale that turns out to be nearly identical to the Kelvin scale is the *ideal-gas temperature scale*. The temperatures on this scale are measured using a *constant-volume gas thermometer* 



Comparison of temperature scales

A comparison of various temperature scales is given in Fig. 1–27

- The reference temperature in the original Kelvin scale was the *ice point*, 273.15 K, which is the temperature at which water freezes (or ice melts).
- The reference point was changed to a much more precisely reproducible point, the *triple point* of water (the state at which all three phases of water coexist in equilibrium), which is assigned the value 273.16 K.



#### **1.9 PRESSURE**

Pressure is defined as **a normal force exerted by a fluid per unit area**. Normally, we speak of pressure when we deal with a gas or a liquid. The counterpart of pressure in solids is **normal stress**. Since pressure is defined as force per unit area, it has the unit of newton's per square meter  $(N/m^2)$ , which is called a *pascal* (Pa)  $1(Pa) = 1 (N/m^2)$ 

1 bar = 10<sup>5</sup> Pa = 0.1 MPa = 100 kPa 1 atm = 101,325 Pa = 101.325 kPa = 1.01325 bars 1 kgf/cm<sup>2</sup> = 9.807 N/cm<sup>2</sup> = 9.807 3 10<sup>4</sup> N/m<sup>2</sup> = 9.807 3 10<sup>4</sup> Pa = 0.9807 bar = 0.9679 atm

The actual pressure at a given position is called the *absolute pressure*, and it is measured relative to absolute vacuum (i.e., absolute zero pressure). Most pressure-measuring devices, however, are calibrated to read zero in the atmosphere (Fig. 1–40), and so they indicate the difference between the absolute pressure and the local atmospheric pressure. This difference is called the *gage pressure*. *P*gage can be positive or negative, but pressures below atmospheric pressure are sometimes called *vacuum pressures* and are measured by vacuum gages that indicate the difference between the atmospheric pressure and the absolute pressure. Absolute, gage, and vacuum pressures are related to each other by

$$P_{gage} = P_{abs} - P_{atm}$$
$$P_{vac} = P_{atm} - P_{abs}$$

This is illustrated in Fig. 1–28



# **Chapter 2** ENERGY ANALYSIS OF CLOSED SYSTEMS

Thermodynamics deals only with the change of the total energy.

The macroscopic forms of energy are those a system possesses as a whole with respect to some outside reference frame, such as kinetic and potential energies (Fig. 2-1).

The microscopic forms of energy are those related to the molecular structure of a system and the degree of the molecular activity, and they are independent of outside reference frames.

Energy can exist in numerous forms such as thermal, mechanical, kinetic, potential, electric, magnetic, chemical, and nuclear, and their sum constitutes the total energy E of a system.

The sum of all the microscopic forms of energy is called the internal energy of a system and is denoted by U.

The energy that a system possesses as a result of its motion relative to some reference frame is called kinetic energy (KE).

The energy that a system possesses as a result of its elevation in a gravitational field is called potential energy (PE).

# potential energy (PE)

PE = mgz (kJ)

or, on a unit mass basis

$$pe = gz$$
 (kJ/kg)

kinetic energy (KE)

$$KE = m \frac{V^2}{2}$$
 (kJ)

or, on a unit mass basis

$$ke = \frac{V^2}{2} \quad (kJ/kg)$$

the total energy of a system consists of the kinetic, potential, and internal energies and is expressed as

 $E = U + KE + PE = U + m\frac{V^2}{2} + mgz$  (kJ)

or, on a unit mass basis

 $e = u + ke + pe = u + \frac{V^2}{2} + gz$  (kJ/kg) Total energy per unit mass  $e = \frac{E}{m}$  (kJ/kg)



#### FIGURE 2–1

The macroscopic energy of an object changes with velocity and elevation.



#### FIGURE 2–2

The various forms of microscopic energies that make up sensible energy

# **4.3 SPECIFIC HEATS**

The specific heat is defined as the energy required to raise the temperature of a unit mass of a substance by one degree (Fig. 2–3).

Specific heat at constant volume,  $c_v$ : The energy required to raise the temperature of the unit mass of a substance by one degree as the volume is maintained constant.

Specific heat at constant pressure,  $c_p$ : The energy required to raise the temperature of the unit mass of a substance by one degree as the pressure is maintained constant.

The specific heat at constant pressure c<sub>p</sub> is always greater than cv because at constant pressure the system is allowed to expand and the energy for this expansion work must also be supplied to the system



#### FIGURE 2–3

Specific heat is the energy required to raise the temperature of a unit mass of a substance by one degree in a specified way

**FIGURE 2–4** Constant-volume and constant pressure specific heats c<sub>v</sub> and c<sub>p</sub> (values given are for helium gas).

- 1. The equations in the figure are valid for any substance undergoing any process.
- 2. cv and cp are properties.
- 3. cv is related to the changes in internal energy and cp to the changes in enthalpy.
- 4. A common unit for specific heats is  $kJ/kg \cdot C$  or  $kJ/kg \cdot K$ . Are these units identical?
- 5. cv = cp = c for solid
- 6.  $cv \cong cp$  for liquid
- 7.  $cv \neq cp$  for gas

The only two forms of energy interactions associated with a closed system are heat transfer and work. The difference between heat transfer and work: An energy interaction is heat transfer if its driving force is a temperature difference. Otherwise it is work.

The mechanical energy can be defined as the form of energy that can be converted to mechanical work completely and directly by an ideal mechanical device such as an ideal turbine. Kinetic and potential energies are the familiar forms of mechanical energy.





Enthalpy: a combination property in many thermodynamics analysis the sum of internal energy (u) and product of pressure (p) and volume (v) operas.

$$\begin{aligned} h &= u + Pv \\ Pv &= RT \end{aligned}$$
 
$$h &= u + RT \\ h &= h(T) \\ du &= c_v(T) dT \\ dh &= c_p(T) dT \end{aligned}$$

$$\Delta h = h_2 - h_1 = \int_1^2 c_p(T) \, dT$$
 (kJ/kg

$$\Delta u = u_2 - u_1 = \int_1^2 c_v(T) \, dT$$
 (kJ/kg

$$u_2 - u_1 = c_{v,avg}(T_2 - T_1)$$
 (kJ/kg)

$$h_2 - h_1 = c_{p,avg}(T_2 - T_1)$$
 (kJ/kg)



0.855 kJ

FIGURE 2–6 The specific heat of a substance changes with temperature



# FIGURE 2–7

For ideal gases, u, h, cv, and cp vary with temperature only.



#### FIGURE 2–8

In the preparation of ideal-gas tables, 0 K is chosen as the reference temperature.



#### FIGURE 2–9

The relation  $\Delta u = C_v \Delta T$  is valid for any kind of process, constant-volume or not.

$$\Delta U = m(u_2 - u_1)$$

$$\Delta \text{KE} = \frac{1}{2} m (V_2^2 - V_1^2)$$

 $\Delta PE = mg(z_2 - z_1)$ 







**FIGURE 2–11** For stationary systems,  $\Delta KE = \Delta PE = 0$ ; thus  $\Delta E = \Delta U$ .

# Chapter 3

# Application of the first law of thermodynamics to flow process (open system)

The **First law of thermodynamics** is simply an expression of the conservation of energy principle, and it asserts that *energy* is a thermodynamic property. Energy cannot be created or destroyed; it can only change forms (the first law). during an integration at system and its surroundings. The amount of energy gained by the system must be exactly equal to the amount pf energy lost be the surrounding. the first law of thermodynamic in mathematical form ( $Q_{net} = W_{net}$ )

# **3.1 ENERGY ANALYSIS OF STEADY-FLOW SYSTEMS**

Many engineering systems such as ( turbines, compressors, nozzles and power plants) operate under steady conditions .



$$\dot{Q} - \dot{W} = \sum_{in} \dot{m} \left( h + \frac{v^2}{2} + gz \right) - \sum_{out} \dot{m} \left( h + \frac{v^2}{2} + gz \right)$$
  
$$\dot{Q} - \dot{W} = \dot{m} \left[ h_2 - h_1 + \frac{v_2^2 - v_1^2}{2} + g(Z_2 - Z_1) \right]$$
(KW)

Where

$$q = \dot{Q}/\dot{m}$$
 and  $w = \dot{W}/\dot{m}$ 

$$q - W = \left[h_2 - h_1 + \frac{V_2^2 - V_1^2}{2} + g(Z_2 - Z_1)\right]$$
 (KJ/Kg)

 $q - w = h_2 - h_1$  when kinetic and potential energy changes are negligible  $\dot{Q}$  =rate of heat transfers between the control volume and its surroundings  $\dot{W}$  = power (KW)

# **3.2 SOME STEADY-FLOW ENGINEERING DEVICES**

#### 1.Turbines

A turbine is a device for extracting work from a flowing fluid expanding from a high pressure to low pressure.

Assumptions

- 1. Neglect heat transfer a cross boundary
- 2. Neglect the variation in potential energy
- 3. Neglect the variation in kinetic energy

Applied these assumptions on SFEE we get

$$\dot{Q} - \dot{W} = \dot{m} \left[ h_2 - h_1 + \frac{V_2^2 - V_1^2}{2} + g(Z_2 - Z_1) \right]$$
  
$$\dot{W} = \dot{m} \left[ h_1 - h_2 \right] \qquad (W + ve)$$

2.Compressors, a rotary compressor may be defined as a reversed turbine doing work on fluid to raise its pressure

Assumptions

- 1. Neglect heat transfer a cross boundary
- 2. Neglect the variation in potential energy
- 3. Neglect the variation in kinetic energy Applied these assumption on SFEE we get

$$\dot{Q} - \dot{W} = \dot{m} \left[ h_2 - h_1 + \frac{V_2^2 - V_1^2}{2} + g(Z_2 - Z_1) \right]$$
  
$$\dot{W} = \dot{m} \left[ h_2 - h_1 \right] \qquad (W - ve)$$

A nozzle is a device that *increases the velocity of a fluid* at the expense of pressure. A **diffuser** is a device that *increases the pressure of a fluid* by slowing it down.

Assumptions

- 1. Neglect heat transfer a cross boundary
- 2. Neglect the variation in potential energy
- 3. Neglect the work W=0

Applied these assumption on SFEE we get

$$\dot{Q} - \dot{W} = \dot{m} \left[ h_2 - h_1 + \frac{v_2^2 - v_1^2}{2} + g(Z_2 - Z_1) \right]$$

$$h_2 + \frac{v_2^2}{2} = h_1 + \frac{v_1^2}{2}$$
For nozzle  $(V_1 < < V_2);$ 

$$V_2 = \sqrt{2(h_1 - h_2)}$$
For diffuser  $(V_2 < < V_1)$ 

$$V_1 = \sqrt{2(h_2 - h_1)}$$



**FIGURE 3–3** Nozzles and diffusers are shaped so that they cause large changes in fluid velocities and thus kinetic energies

#### 5. Throttling Valves

Throttling is one of important process in thermal engineering. It used for reducing their pressure without decreasing the energy of fluid. Throttles may or may not be insulate but more time take adiabatic device for throttle valve Q=0, W=0,  $\Delta Z = 0$ , K.E and P.E neglected then from SFEE yields.

$$\dot{Q} - \dot{W} = \dot{m} \left[ h_2 - h_1 + \frac{V_2^2 - V_1^2}{2} + g(Z_2 - Z_1) \right]$$
  
 $h_2 = h_1$ 

#### 6.Boilers

For boilers; work exchange is zero,  $\Delta PE d \Delta KEan$  is also zero, then from SFEE yields .

$$\dot{Q} - \dot{W} = \dot{m} \left[ h_2 - h_1 + \frac{V_2^2 - V_1^2}{2} + g(Z_2 - Z_1) \right]$$
  
 $\dot{Q} = \dot{m} (h_1 - h_2)$  always (Q +Ve)

#### 7.Condensers

For condensers; work exchange is zero,  $\Delta PE d \Delta KE$  an is also zero, then from SFEE yields .

$$\dot{Q} - \dot{W} = \dot{m} \left[ h_2 - h_1 + \frac{V_2^2 - V_1^2}{2} + g(Z_2 - Z_1) \right]$$
  
 $\dot{Q} = \dot{m} (h_2 - h_1)$  always (Q - Ve)

In engineering applications, the section where the mixing process takes place is commonly referred to as a **mixing chamber**.

#### 8. Mixing Chambers

Energy balance for the adiabatic mixing chamber in the figure is

 $\dot{E}_{in} = \dot{E}_{out}$   $\dot{m}_1 h_1 + \dot{m}_2 h_2 = \dot{m}_3 h_3$ (since  $\dot{Q} \approx 0, \dot{W} = 0, \text{ke} \approx \text{pe} \approx 0$ )  $\dot{m}_1 h_1 + \dot{m}_2 h_2 = (\dot{m}_1 + \dot{m}_2) h_3$ 

# **3.3 FLOW WORK AND THE ENERGY OF A FLOWING FLUID**

Flow work, or flow energy: The work (or energy) required to push the mass into or out of the control volume. This



(a) An adjustable valve



(c) A capillary tube

**FIGURE 3–4** Throttling valves are devices that cause large pressure drops in the fluid.



FIGURE 3–5 Boilers



FIGURE 3–6 condensers

work is necessary for maintaining a continuous flow through a control volume.





**FIGURE 3-9** In the absence of acceleration, the force applied on a fluid by a piston is equal to the force applied on the piston by the fluid.



**FIGURE 3–10** The T-elbow of an ordinary shower serves as the mixing chamber for the hot- and the cold-water streams.



**FIGURE 3–11** During a steadyflow process, volume flow rates are not necessarily conserved although mass flow rates are.

#### **MOVING BOUNDARY WORK**

one form of mechanical work frequently encountered in practice is associated with the expansion or compression of a gas in a pistoncylinder device. During this process, part of the boundary (the inner face of the piston) moves back and forth. Therefore, the expansion and compression work is often called **moving boundary work**, or simply **boundary work** (Fig. 3–12). (Some call it the  $P \, dV$  work for reasons explained later. Moving boundary work is the primary form of work involved in *automobile engines*. During their expansion, the combustion gases force the piston to move, which in turn forces the crankshaft to rotate.

$$\delta W_h = F \, ds = PA \, ds = P \, dV$$

$$W_b = \int_1^2 P dV \quad \text{(kJ)}$$

Quasi-equilibrium process: A process during which the system

- remains nearly in equilibrium at all times.
- $W_b$  is positive  $\rightarrow$  for expansion
- $W_b$  is negative  $\rightarrow$  for compression



#### FIGURE 3–13

The area under the process curve on a *P*-*V* diagram represents the boundary work

Area = 
$$A = \int_{1}^{2} dA = \int_{1}^{2} P dV$$



**FIGURE 3–14** The boundary work done during a process depends on the path followed as well as the end states.



#### FIGURE 3–12

The work associated with a moving boundary is called *boundary work* 



# FIGURE 3–15

A gas does a differential amount of work  $dW_b$  as it forces the piston to move by a differential amount ds

# 3.4 First law thermodynamic applied to non-flow process (closed system )

Assumptions.

- 1. Reversible process
- 2. quasi-equilibrium
- 3. Displacement work
- 4. Kinetic energy and potential energy are neglected

General analysis for a closed system undergoing a constant-pressure process.



#### The non-flow process are

#### **1.constant volume process**

From non flow energy (NFEE)

 $Q-W=\Delta U$  $W_{b} = \int^{2} P \, d\vec{V} = 0$ 

W=0

$$Q = \Delta U$$

#### 2.constant pressure process

From non flow energy (NFEE) Q-W= $\Delta U$   $W_b = \int_1^2 P dV = P_0 \int_1^2 dV = P_0(V_2 - V_1)$   $Q - W_{other} - P_0(V_2 - V_1) = U_2 - U_1$   $P_0 = P_2 = P_1 \rightarrow Q - W_{other} = (U_2 + P_2V_2) - (U_1 + P_1V_1)$ Also H = U + PV, and thus

$$Q - W_{\text{other}} = H_2 - H_1 \quad \text{(kJ)}$$



**FIGURE 3–16** Schematic and P-v diagram for constant volume.



# **3.constant temperature process**

From non flow energy (NFEE)

 $Q-W=\Delta U$   $\Delta U = 0$  Q = W $PV = mRT_0 = C \text{ or } P = \frac{C}{V}$ 

$$W_b = \int_1^2 P \, dV = \int_1^2 \frac{C}{V} dV = C \int_1^2 \frac{dV}{V} = C \ln \frac{V_2}{V_1} = P_1 V_1 \ln \frac{V_2}{V_1}$$

# 4.polytropic process

 $Pv^n = c$ 

 $P = CV^{-n}$ 

$$W_b = \int_1^2 P \, dV = \int_1^2 C V^{-n} \, dV = C \, \frac{V_2^{-n+1} - V_1^{-n+1}}{-n+1} = \frac{P_2 V_2 - P_1 V_1}{1-n}$$

since  $C = P_1 V_1^n = P_2 V_2^n$ . For an ideal gas (PV = mRT), this equation can also be written as

$$W_b = \frac{mR(T_2 - T_1)}{1 - n}$$
  $n \neq 1$  (kJ)



**FIGURE 3–18** Schematic and *P-V* diagram for a polytropic process.

Process	General	Heat energy	Work energy	Combination of
	law			process with
				characteristic
				equation of gas
Constant	V=C	$Q=\Delta U=mC_v\Delta T$	W=0	$\frac{PV}{T} = C, \frac{P_1V_1}{T} = \frac{P_2V_2}{T},$
volume				$\begin{array}{cccc} T & T_1 & T_2 \\ P_1 & P_2 & D & C \\ \end{array}$
				$\frac{1}{T_1} = \frac{1}{T_2},  \mathbf{R} = \mathbf{C}_{\mathbf{P}} - \mathbf{C}_{\mathbf{V}}$
Constant	P=C	$\mathbf{Q} = \Delta H = m C_P \Delta T$	W=P( $V_2 - V_1$ )	$\frac{PV}{P} = C \cdot \frac{P_1V_1}{P_2V_2} = \frac{P_2V_2}{P_2V_2}$
pressure				$T$ $T_1$ $T_2$
				$\frac{T_1}{T_1} = \frac{T_2}{T_2}, R = C_P - C_V$
Isothermal	T=C	$\mathbf{O} = \mathbf{P}_1 \mathbf{V}_1 \ln \frac{\mathbf{V}_2}{\mathbf{V}_1}$	$O = P_1 V_1 \ln \frac{V_2}{V_1}$	PV=C
process	PV=C	$v = 1 \cdot 1 \cdots v_1$		
		Vr	Ur Va	$P_1V_1 = P_2V_2$
		$Q=mRTln\frac{12}{V_1}$	W=mRTIn $\frac{V_2}{V_1}$	
		Or	Or	$\mathbf{R} = \mathbf{C}_{\mathbf{P}} - \mathbf{C}_{\mathbf{V}}$
		$O=mRTln\frac{P_1}{2}$	W=mRTln $\frac{P_1}{2}$	
		e P <sub>2</sub>	P <sub>2</sub>	
Polytropic	$\mathbf{P}\mathbf{V}^{\mathbf{n}}-\mathbf{C}$	0	$P_1V_1 - P_2V_2$	$PV = P_1V_1 = P_2V_2$
nrocess	IV -C	$\gamma - n$	$W = \frac{n-1}{n-1}$	$\frac{1}{T} = C, \frac{1}{T_1} = \frac{1}{T_2}$
process		$=\frac{1}{\nu-1\delta}$ ×polytropic work		$\mathbf{P} \cdot \mathbf{V} \cdot \mathbf{n} = \mathbf{P} \cdot \mathbf{V} \cdot \mathbf{n}$
		1 10	$W = \frac{mR(T_1 - T_2)}{mR(T_1 - T_2)}$	
			<i>n</i> -1	$\frac{P_2}{r} = (\frac{V_1}{r})^n$ ,
				$P_1  V_2$
				$\frac{T_2}{T_2} = (\frac{V_1}{V_1})^{n-1}$
				$T_1^{-}V_2^{\prime}$
				$T_2 P_2 n-1$
				$\frac{2}{T_{\star}} = \left(\frac{2}{P_{\star}}\right)^{n}$
				$\mathbf{R} = \mathbf{C}\mathbf{P} - \mathbf{C}\mathbf{V}$
Adiabatic	$PV^{\gamma}=C$	Q=0	$W - \frac{P_1V_1 - P_2V_2}{P_1V_1 - P_2V_2}$	$\frac{PV}{P} = C \cdot \frac{P_1V_1}{P_2V_2} = \frac{P_2V_2}{P_2V_2}$
process			γ-1 γ-1	$T$ $T_1$ $T_2$
				$P_1 V_1^{\gamma} = P_2 V_2^{\gamma}$
			$W = \frac{mR(T_1 - T_2)}{mR(T_1 - T_2)}$	$P_2 = V_{1,N}$
			γ-1	$\frac{1}{P_1} = \left(\frac{1}{V_2}\right)^{\gamma} ,$
				$\left \frac{T_2}{T}\right  = \left(\frac{V_1}{V}\right)^{\gamma-1}$
				$I_1 V_2$
				$\left \frac{T_2}{T_2}-\frac{P_2}{V}\right ^{\frac{\gamma-1}{\gamma}}$
				$\overline{T_1} - (\overline{P_1})'$
				$\mathbf{K} = \mathbf{C}_{\mathbf{P}} - \mathbf{C}_{\mathbf{V}}, \boldsymbol{\gamma} = \frac{\mathbf{r}}{c_{v}}$
1	1		1	1

# **Chapter 4 PROPERTIES OF PURE SUBSTANCES**

# **4.1 PURE SUBSTANCE**

A substance that has a fixed chemical composition throughout is called a pure substance. Water, nitrogen, helium, and carbon dioxide, for example, are all pure substances.



# 4.2 PHASE-CHANGE PROCESSES OF PURE SUBSTANCES

Consider a piston–cylinder device containing liquid water at 20 <sup>o</sup>C and 1 atm pressure (state 1, Fig. 4–3). Under these conditions, water exists in the liquid phase, and it is called a compressed liquid, or a subcooled liquid, meaning that it is not about to vaporize.

As more heat is transferred, the temperature keeps rising until it reaches 100<sup>o</sup>C (state 2, Fig. 4–4). At this point water is still a liquid, but any heat addition will cause some of the liquid to vaporize. That is, a phase-change process from liquid to vapor is about to take place. A liquid that is about to vaporize is called a saturated liquid. Therefore, state 2 is a saturated liquid state.



FIGURE 4–3	FIGURE
At 1 atm and	1 atm pre
$20^{\circ}$ C, water exists	and 100°C
in the liquid	exists as a
phase(compressed	that is rea
liquid).	vaporize(
	liquid).

FIGURE 4–4 At 1 atm pressure and  $100^{\circ}$ C water exists as a liquid that is ready to vaporize(saturated iquid).

#### FIGURE 4–5 As more heat is transferred, part of the saturated liquid vaporizes (saturated liquid–vapor mixture).

**FIGURE 4–6** At 1 atm pressure, the temperature remains constant at 100 <sup>0</sup>C until the last drop of liquid is vaporized (saturated vapor)

As more heat is transferred, the temperature of the vapor starts to rise (superheated vapor).

FIGURE 4–7

A vapor that is about to condense is called a saturated vapor.

saturated liquid-vapor mixture since the liquid and vapor phases coexist in equilibrium at these states.

A vapor that is not about to condense (i.e., not a saturated vapor) is called a superheated vapor.

The temperature at which water starts boiling depends on the pressure; therefore, if the pressure is fixed, so is the boiling temperature. Water boils at  $100^{\circ}$ C at 1 atm pressure.

At a given pressure, the temperature at which a pure substance changes phase is called the saturation temperature  $T_{sat}$ . Likewise, at a given temperature, the pressure at which a pure substance changes phase is called the saturation pressure  $P_{sat}$ .

If the entire process between state 1 and 5 described in the figure is reversed by cooling the water while maintaining the pressure at the same value, the water will go back to state 1, retracing the same path, and in so doing, the amount of heat released will exactly match the amount of heat added during the heating process.

#### TABLE 3-1

Saturation (or vapor) pressure of water at various temperatures

Temperature	Saturation Pressure	
7, 0	/ sat, Ki d	
-10	0.260	
-5	0.403	
0	0.611	
5	0.872	
10	1.23	
15	1.71	
20	2.34	
25	3.17	
30	4.25	
40	7.38	
50	12.35	
100	101.3 (1 atm)	
150	475.8	
200	1554	
250	3973	
300	8581	

The amount of energy absorbed or released during a phase-change process is called the latent heat. More specifically, the amount of energy absorbed during melting is called the latent heat of fusion and is equivalent to the amount of energy released during freezing. Similarly, the amount of energy absorbed during vaporization is called the latent heat of vaporization and is equivalent to the energy released during condensation.

The magnitudes of the latent heats depend on the temperature or pressure at which the phase change occurs.



**FIGURE 4–9** The liquid–vapor saturation curve of a pure substance (numerical values are for water).

TABLE 2 2									
TABLE 3-2									
Variation of the standard atmospheric pressure and the boiling (saturation) temperature of water with altitude									
Elevation, m	Boiling tempera- ture, °C								
0 1,000 2,000 5,000 10,000 20,000	101.33 89.55 79.50 54.05 26.50 5.53	100.0 96.5 93.3 83.3 66.3 34.7							

At 1 atm pressure, the latent heat of fusion of water is 333.7 kJ/kg and the latent heat of vaporization is 2256.5 kJ/kg.

The atmospheric pressure, and thus the boiling temperature of water, decreases with elevation.

# 4.3 PROPERTY DIAGRAMS FOR PHASE-CHANGE PROCESSES

# 1 The T-v Diagram

As the pressure is increased further, this saturation line continues to shrink, as shown in Fig. 3–15, and it becomes a point when the pressure reaches 22.06 MPa for the case of water. This point is called the critical point, and it is defined as the point at which the saturated liquid and saturated vapor states are identical. The saturated liquid states in Fig. 4-**10** can be connected by a line called the saturated liquid line, and saturated vapor states in the same figure can be connected by another line, called the saturated vapor line



#### FIGURE 4–10



These two lines meet at the critical point, forming a dome as shown in Fig. 4–11a. All the compressed liquid states are located in the region to the left of the saturated liquid line, called the compressed liquid region. All the superheated vapor states are located to the right of the saturated vapor line, called the superheated vapor region. In these two regions, the substance exists in a single phase, a liquid or a vapor. All the states that involve both phases in equilibrium are located under the dome, called the saturated liquid–vapor mixture region, or the wet region.



# 4.4 PROPERTY TABLES

For most substances, the relationships among thermodynamic properties are too complex to be expressed by simple equations. Therefore, properties are frequently presented in the form of tables. Some thermodynamic properties can be measured easily, but others cannot and are calculated by using the relations between them and measurable properties. The results of these measurements and calculations are presented in tables in a convenient format. Before we get into the discussion of property tables, we define a new property called enthalpy.

# 1a Saturated Liquid and Saturated Vapor States



**FIGURE 4–12** A partial list of Table A–4.



**FIGURE 4–13** The product pressure × volume has energy units.

 $v_f$  = specific volume of saturated liquid

 $v_g$  = specific volume of saturated vapor

 $v_{fg}$  = difference between  $v_g$  and  $v_f$  (that is  $v_{fg} = v_g - v_f$ )

The quantity  $h_{fg}$  is called the enthalpy of vaporization (or latent heat of vaporization). It represents the amount of energy needed to vaporize a unit mass of saturated liquid at a given temperature or pressure. It decreases as the temperature or pressure increases and becomes zero at the critical point.

# 1b Saturated Liquid–Vapor Mixture

Quality, x : The ratio of the mass of vapor to the total mass of the mixture. Quality is between 0 and 1 (0: sat. liquid), (1: sat. vapor)

The properties of the saturated liquid are the same whether it exists alone or in a mixture with saturated vapor.

 $P \text{ or } T^{\bigstar}$ 



Temperature and pressure are dependent properties for a mixture





**FIGURE 4–15** Quality is related to the horizontal distances on P-v and T-v diagrams.



**FIGURE 4–14** The relative amounts of liquid and vapor phases in a saturated mixture are specified by the quality x.

**FIGURE 4–16** A two-phase system can be treated as a homogeneous mixture for convenience.

# **2** Superheated Vapor

In the region to the right of the saturated vapor line and at temperatures above the critical point temperature, a substance exists as superheated vapor. In this region, temperature and pressure are independent properties.

Compared to saturated vapor, superheated vapor is characterized by

Lower pressures  $(P < P_{sat} \text{ at a given } T)$ Higher tempreatures  $(T > T_{sat} \text{ at a given } P)$ Higher specific volumes  $(v > v_g \text{ at a given } P \text{ or } T)$ Higher internal energies  $(u > u_g \text{ at a given } P \text{ or } T)$ Higher enthalpies  $(h > h_g \text{ at a given } P \text{ or } T)$ 

#### **3** Compressed Liquid

The compressed liquid properties depend on temperature much more strongly than they do on pressure.

 $y \cong y_{f@T}$ 

$$\mathbf{y} \rightarrow \mathbf{v}, \, \mathbf{u}, \, \mathrm{or}$$

A more accurate relation for h $h \cong h_{f@T} + v_{f@T} (P - P_{sat @T})$ 

```
Given: P and T

\lor \cong \lor_{f \otimes T}

u \cong u_{f \otimes T}

h \cong h_{f \otimes T}

\circ \circ @
```

#### FIGURE 4–17

A compressed liquid may be approximated as a saturated liquid at the given temperature. In general, a compressed liquid is characterized by Higher pressures ( $P > P_{sat}$  at a given T) Lower tempreatures ( $T < T_{sat}$  at a given P) Lower specific volumes ( $v < v_f$  at a given P or T) Lower internal energies ( $u < u_f$  at a given P or T) Lower enthalpies ( $h < h_f$  at a given P or T)

0				
0				
		v	и	h
	T,°C	m <sup>3</sup> /kg	kJ/kg	kJ/kg
		P = 0.1	MPa (99.	61°C)
_	Sat.	1.6941	2505.6	2675.0
	100	1.6959	2506.2	2675.8
0	150	1.9367	2582.9	2776.6
~				
	1300	7.2605	4687.2	5413.3
		P = 0.5	MPa (151	.83°C)
	Sat.	0.37483	2560.7	2748.1
	200	0.42503	2643.3	2855.8
0	250	0.47443	2723.8	2961.0
~				
0				

**FIGURE 4–18** A partial listing of Table A–6



#### **FIGURE 4–19**

At a specified P, superheated vapor exists at a higher h than the saturated vapor (Example 3–7).

		<i>Specific volume,</i> m <sup>3</sup> /kg		/	Internal energy, kJ/kg		Enthalpy, kJ/kg			<i>Entropy,</i> kJ/kg · К		
Temp., <i>T</i> °C	Sat. press., <i>P<sub>sat</sub></i> kPa	Sat. liquid, v <sub>f</sub>	Sat. vapor, v <sub>g</sub>	Sat. Iiquid, <i>u<sub>f</sub></i>	Evap., <i>u<sub>fg</sub></i>	Sat. vapor, u <sub>g</sub>	Sat. Iiquid, <i>h<sub>f</sub></i>	Evap., <i>h<sub>fg</sub></i>	Sat. vapor, <i>h<sub>g</sub></i>	Sat. liquid, <i>s</i> f	Evap., <i>s<sub>fg</sub></i>	Sat. vapor, <i>s<sub>g</sub></i>
0.01 5	0.6117 0.8725	0.001000 0.001000	206.00 147.03	0.000 21.019	2374.9 2360.8	2374.9 2381.8	0.001 21.020	2500.9 2489.1	2500.9 2510.1	0.0000 0.0763	9.1556 8.9487	9.1556 9.0249

Saturated water—Temperature table

Saturated refrigerant-134a—Temperature table

<i>Specific volu</i> m <sup>3</sup> /kg		volume, Kg	Internal energy, kJ/kg			Enthalpy, kJ/kg			<i>Entropy,</i> kJ/kg · К			
Temp. <i>T</i> °C	Sat. , press., <i>P<sub>sat</sub></i> kPa	Sat. liquid, v <sub>f</sub>	Sat. vapor, <i>v<sub>g</sub></i>	Sat. liquid, <i>u<sub>f</sub></i>	Evap., <i>u<sub>fg</sub></i>	Sat. vapor, <i>u<sub>g</sub></i>	Sat. liquid, <i>h<sub>f</sub></i>	Evap., h <sub>fg</sub>	Sat. vapor, <i>h<sub>g</sub></i>	Sat. Iiquid, <i>s<sub>f</sub></i>	Evap., s <sub>fg</sub>	Sat. vapor, <i>s<sub>g</sub></i>
-40	51.25	0.0007054	0.36081	-0.036	207.40	207.37	0.000	225.86	225.86	0.00000	0.96866	0.96866

# 4.5 THE IDEAL-GAS EQUATION OF STATE

Any equation that relates the pressure, temperature, and specific volume of a substance is called an equation of state.

The simplest and best-known equation of state for substances in the gas phase is the ideal-gas equation of state. This equation predicts the P-v-T behavior of a gas quite accurately within some properly selected region.

$$P = R\left(\frac{T}{v}\right)$$

$$R = \frac{R_u}{M}$$
(kJ/kg·K or kPa·m<sup>3</sup>/kg·K)

where  $R_u$  is the universal gas constant and M is the molar mass (also called molecular weight) of the gas. The constant  $R_u$  is the same for all substances, and its value is

$$R_{u} = \begin{cases} 8.31447 \text{ kJ/kmol} \cdot \text{K} \\ 8.31447 \text{ kPa} \cdot \text{m}^{3}/\text{kmol} \cdot \text{K} \\ 0.0831447 \text{ bar} \cdot \text{m}^{3}/\text{kmol} \cdot \text{K} \\ 1.98588 \text{ Btu/lbmol} \cdot \text{R} \\ 10.7316 \text{ psia} \cdot \text{ft}^{3}/\text{lbmol} \cdot \text{R} \\ 1545.37 \text{ ft} \cdot \text{lbf/lbmol} \cdot \text{R} \end{cases}$$

The molar mass M can simply be defined as the mass of one mole (also called a gram-mole, abbreviated gmol) of a substance in grams, or the mass of one kmol (also called a kilogram-mole,

Substance	_R, kJ/kg·K_
Air Helium	0.2870
Argon	0.2081
Nitrogen	0.2968
	000

#### FIGURE 4–20

Different substances have different gas constants.

abbreviated kgmol) in kilograms. In English units, it is the mass of 1 lbmol in lbm.

 $Mass = Molar mass \times Mole number$ 

m = MN(kg)  $\frac{P_1 V_1}{T_1} = \frac{P_2 V_2}{T_2}$ 

Ideal gas equation at two states for a fixed mass

$$V = mv \longrightarrow PV = mRT$$

 $mR = (MN)R = NR_u \longrightarrow PV = NR_uT$ 

$$V = N\overline{v} \longrightarrow P\overline{v} = R_{\mu}T$$

Various expressions of ideal gas equation Real gases behave as an ideal gas at low densities (i.e., low pressure, high temperature).

P	Per unit mass	Per unit mole	
	v, m <sup>3</sup> /kg	⊽, m <sup>3</sup> /kmol	
	u, kJ/kg	$\overline{u}$ , kJ/kmol	
	h, kJ/kg	h, kJ/kmol	
4.			

#### **FIGURE 4–21** Properties per unit mole are

denoted with a bar on the top

#### Properties of common liquids, solids, and foods

(a) Liquids

	Boiling data at 1 atm		Freez	ing data	Liquid properties			
Substance	Normal boiling point, °C	Latent heat of vaporization h <sub>fg</sub> , kJ/kg	Freezing point, °C	Latent heat of fusion h <sub>if</sub> , kJ/kg	Temperature, ℃	Density $ ho$ , kg/m <sup>3</sup>	Specific heat c <sub>p</sub> , kJ/kg·K	
Ammonia	-33.3	1357	-77.7	322.4	-33.3	682	4.43	
					-20	665	4.52	
					0	639	4.60	
					25	602	4.80	
Argon	-185.9	161.6	-189.3	28	-185.6	1394	1.14	
Benzene	80.2	394	5.5	126	20	879	1.72	
Brine (20% sodium	100.0							
chloride by mass)	103.9	—	-17.4	_	20	1150	3.11	
<i>n</i> -Butane	-0.5	385.2	-138.5	80.3	-0.5	601	2.31	
Carbon dioxide	- /8.4*	230.5 (at 0°C)	-56.6	100	0	298	0.59	
Ethanol	78.2	838.3	-114.2	109	25	/83	2.46	
Ethyl alconol	/8.6	800 1	-156	108	20	/89	2.84	
Chroning	190.1	000.1	-10.8	200.6	20	1261	2.04	
Holium	-268.9	22.8	10.9	200.0	-268.9	146.2	2.32	
Hydrogen	-252.8	445.7	-259.2	59.5	-252.8	70.7	10.0	
Isobutane	-117	367.1	-160	105.7	-117	593.8	2.28	
Kerosene	204-293	251	-24.9		20	820	2.20	
Mercury	356.7	294.7	-38.9	11.4	25	13.560	0.139	
Methane	-161.5	510.4	-182.2	58.4	-161.5	423	3.49	
					-100	301	5.79	
Methanol	64.5	1100	-97.7	99.2	25	787	2.55	
Nitrogen	-195.8	198.6	-210	25.3	-195.8	809	2.06	
					-160	596	2.97	
Octane	124.8	306.3	-57.5	180.7	20	703	2.10	
Oil (light)					25	910	1.80	
Oxygen	-183	212.7	-218.8	13.7	-183	1141	1.71	
Petroleum	—	230-384			20	640	2.0	
Propane	-42.1	427.8	-187.7	80.0	-42.1	581	2.25	
					0	529	2.53	
D ( )	0.5.1	017.0	000		50	449	3.13	
Refrigerant-134a	-26.1	217.0	-96.6	—	-50	1443	1.23	
					-26.1	1374	1.27	
					25	1295	1.34	
Wator	100	2257	0.0	222.7	25	1207	1.45	
Water	100	2237	0.0	555.7	25	997	4.22	
					50	988	4.18	
					75	975	4.19	
					100	958	4.22	

\* Sublimation temperature. (At pressures below the triple-point pressure of 518 kPa, carbon dioxide exists as a solid or gas. Also, the freezing-point temperature of carbon dioxide is the triple-point temperature of -56.5°C.)

#### Properties of common liquids, solids, and foods (Concluded)

(b) Solids (values are for	b) Solids (values are for room temperature unless indicated otherwise)											
Substance	Density, $\rho$ kg/m <sup>3</sup>	Specific heat, c <sub>p</sub> kJ/kg⋅K	Substance	Density, $\rho \ {\rm kg/m^3}$	Specific heat, c <sub>p</sub> kJ/kg⋅K							
Metals			Nonmetals									
Aluminum			Asphalt	2110	0.920							
200 K		0.797	Brick, common	1922	0.79							
250 K		0.859	Brick, fireclay (500°C)	2300	0.960							
300 K	2,700	0.902	Concrete	2300	0.653							
350 K		0.929	Clay	1000	0.920							
400 K		0.949	Diamond	2420	0.616							
450 K		0.973	Glass, window	2700	0.800							
500 K		0.997	Glass, pyrex	2230	0.840							
Bronze (76% Cu, 2% Zn,	8,280	0.400	Graphite	2500	0.711							
2% AI)			Granite	2700	1.017							
Brass, yellow (65% Cu, 35% Zn)	8,310	0.400	Gypsum or plaster board Ice	800	1.09							
Copper			200 K		1.56							
-173°C		0.254	220 K		1.71							
-100°C		0.342	240 K		1.86							
-50°C		0.367	260 K		2.01							
0°C		0.381	273 K	921	2.11							
27°C	8,900	0.386	Limestone	1650	0.909							
100°C		0.393	Marble	2600	0.880							
200°C		0.403	Plywood (Douglas Fir)	545	1.21							
Iron	7,840	0.45	Rubber (soft)	1100	1.840							
Lead	11,310	0.128	Rubber (hard)	1150	2.009							
Magnesium	1,730	1.000	Sand	1520	0.800							
Nickel	8,890	0.440	Stone	1500	0.800							
Silver	10,470	0.235	Woods, hard (maple, oak, etc.)	721	1.26							
Steel, mild	7,830	0.500	Woods, soft (fir, pine, etc.)	513	1.38							
Tungsten	19,400	0.130										

#### (c) Foods

	Water	_	<i>Specifi</i> kJ/kg	<i>c heat,</i> K	Latent		Watar		<i>Specifi</i> kJ/kg	<i>c heat,</i> ∙K	Latent
Food	content, % (mass)	Freezing point, °C	Above freezing	Below freezing	fusion, kJ/kg Food		content, % (mass)	Freezing point, °C	Above freezing	Below freezing	fusion, kJ/kg
Apples	84	-1.1	3.65	1.90	281	Lettuce	95	-0.2	4.02	2.04	317
Bananas	75	-0.8	3.35	1.78	251	Milk, whole	88	-0.6	3.79	1.95	294
Beef round	67	_	3.08	1.68	224 Oranges		87	-0.8	3.75	1.94	291
Broccoli	90	-0.6	3.86	1.97	301	Potatoes	78	-0.6	3.45	1.82	261
Butter	16	_	_	1.04	53	Salmon fish	64	-2.2	2.98	1.65	214
Cheese, swiss	39	-10.0	2.15	1.33	130	Shrimp	83	-2.2	3.62	1.89	277
Cherries	80	-1.8	3.52	1.85	267	Spinach	93	-0.3	3.96	2.01	311
Chicken	74	-2.8	3.32	1.77	247	Strawberries	90	-0.8	3.86	1.97	301
Corn, sweet	74	-0.6	3.32	1.77	247	Tomatoes, ripe	94	-0.5	3.99	2.02	314
Eggs, whole	74	-0.6	3.32	1.77	247	Turkey	64	_	2.98	1.65	214
Ice cream	63	-5.6	2.95	1.63	210	Watermelon	93	-0.4	3.96	2.01	311

Source of Data: Values are obtained from various handbooks and other sources or are calculated. Water content and freezing-point data of foods are from ASHRAE, Handbook of Fundamentals, SI version (Atlanta, GA: American Society of Heating, Refrigerating and Air-Conditioning Engineers, Inc., 1993), Chapter 30, Table 1. Freezing point is the temperature at which freezing starts for fruits and vegetables, and the average freezing temperature for other foods.

Saturated water—Temperature table

		Specific	c volume,	Inte	ernal ene	rgy,		Enthalpy,			Entropy	;
		m	°/kg		kJ/kg			kJ/kg			kJ/kg∙K	
_	Sat.	Sat.	Sat.	Sat.	_	Sat.	Sat.	_	Sat.	Sat.	_	Sat.
Temp.,	press.,	liquid,	vapor,	liquid,	Evap.,	vapor,	liquid,	Evap.,	vapor,	liquid,	Evap.,	vapor,
7 ℃	P <sub>sat</sub> kPa	V <sub>f</sub>	Vg	Uf	U <sub>fg</sub>	Ug	h <sub>f</sub>	h <sub>fg</sub>	h <sub>g</sub>	Sf	S <sub>fg</sub>	Sg
0.01	0.6117	0.001000	206.00	0.000	2374.9	2374.9	0.001	2500.9	2500.9	0.0000	9.1556	9.1556
10	0.8725	0.001000	147.03	42 020	2360.8	2381.8	42 022	2489.1	2510.1	0.0763	8.9487	9.0249
15	1.7057	0.001000	77.885	62.980	2340.0	2395.5	62.982	2465.4	2528.3	0.2245	8.5559	8.7803
20	2.3392	0.001002	57.762	83.913	2318.4	2402.3	83.915	2453.5	2537.4	0.2965	8.3696	8.6661
25	3.1698	0.001003	43.340	104.83	2304.3	2409.1	104.83	2441.7	2546.5	0.3672	8.1895	8.5567
30	4.2469	0.001004	32.879	125.73	2290.2	2415.9	125.74	2429.8	2555.6	0.4368	8.0152	8.4520
35	5.6291	0.001006	25.205	146.63	2276.0	2422.7	146.64	2417.9	2564.6	0.5051	7.8466	8.3517
40	7.3851	0.001008	19.515	167.53	2261.9	2429.4	167.53	2406.0	25/3.5	0.5724	7.6832	8.2556
40	9.0900	0.001010	10.201	100.45	2247.7	2430.1	100.44	2394.0	2002.4	0.0300	7.5247	0.1033
50	12.352	0.001012	9 5639	209.33	2233.4	2442.7	209.34	2369.8	2591.3	0.7038	7 2218	8.0748 7.9898
60	19.947	0.001017	7.6670	251.16	2204.7	2455.9	251.18	2357.7	2608.8	0.8313	7.0769	7.9082
65	25.043	0.001020	6.1935	272.09	2190.3	2462.4	272.12	2345.4	2617.5	0.8937	6.9360	7.8296
70	31.202	0.001023	5.0396	293.04	2175.8	2468.9	293.07	2333.0	2626.1	0.9551	6.7989	7.7540
75	38.597	0.001026	4.1291	313.99	2161.3	2475.3	314.03	2320.6	2634.6	1.0158	6.6655	7.6812
80	47.416	0.001029	3.4053	334.97	2146.6	2481.6	335.02	2308.0	2643.0	1.0756	6.5355	7.6111
85	57.868	0.001032	2.8261	355.96	2131.9	2487.8	356.02	2295.3	2651.4	1.1346	6.4089	7.5435
95	84.609	0.001030	1.9808	398.00	2102.0	2500.1	398.09	2269.6	2667.6	1.2504	6.1647	7.4151
100	101 42	0.001043	1 6720	419.06	2087.0	2506.0	419 17	2256.4	2675.6	1 3072	6 0470	7 3542
105	120.90	0.001047	1.4186	440.15	2071.8	2511.9	440.28	2243.1	2683.4	1.3634	5.9319	7.2952
110	143.38	0.001052	1.2094	461.27	2056.4	2517.7	461.42	2229.7	2691.1	1.4188	5.8193	7.2382
115	169.18	0.001056	1.0360	482.42	2040.9	2523.3	482.59	2216.0	2698.6	1.4737	5.7092	7.1829
120	198.67	0.001060	0.89133	503.60	2025.3	2528.9	503.81	2202.1	2706.0	1.5279	5.6013	7.1292
125	232.23	0.001065	0.77012	524.83	2009.5	2534.3	525.07	2188.1	2713.1	1.5816	5.4956	7.0771
130	270.28	0.001070	0.66808	546.10	1993.4	2539.5	546.38	21/3./	2720.1	1.6346	5.3919	7.0265
140	361.53	0.001075	0.50850	588.77	1960.9	2549.6	589.16	2144.3	2720.5	1.7392	5.1901	6.9294
145	415.68	0.001085	0.44600	610.19	1944.2	2554.4	610.64	2129.2	2739.8	1.7908	5.0919	6.8827
150	476.16	0.001091	0.39248	631.66	1927.4	2559.1	632.18	2113.8	2745.9	1.8418	4.9953	6.8371
155	543.49	0.001096	0.34648	653.19	1910.3	2563.5	653.79	2098.0	2751.8	1.8924	4.9002	6.7927
160	618.23	0.001102	0.30680	674.79	1893.0	2567.8	675.47	2082.0	2757.5	1.9426	4.8066	6.7492
165	700.93	0.001108	0.27244	696.46	1875.4	2571.9	697.24	2065.6	2762.8	1.9923	4.7143	6.7067
170	792.18	0.001114	0.24260	718.20	1857.5	2575.7	719.08	2048.8	2767.9	2.0417	4.6233	0.0000
1/5	892.60	0.001121	0.21659	740.02	1839.4	25/9.4	741.02	2031.7	2772.7	2.0906	4.5335	6.5841
185	1123.5	0.001127	0.17390	783.91	1802.1	2586.0	785.19	1996.2	2781.4	2.1875	4.3572	6.5447
190	1255.2	0.001141	0.15636	806.00	1783.0	2589.0	807.43	1977.9	2785.3	2.2355	4.2705	6.5059
195	1398.8	0.001149	0.14089	828.18	1763.6	2591.7	829.78	1959.0	2788.8	2.2831	4.1847	6.4678
200	1554.9	0.001157	0.12721	850.46	1743.7	2594.2	852.26	1939.8	2792.0	2.3305	4.0997	6.4302

Saturate	aturated water—Temperature table (Concluded)												
		Specific m <sup>3</sup>	: <i>volume,</i> ³/kg	Inte	ernal ene kJ/kg	rgy,		<i>Enthalpy,</i> kJ/kg			<i>Entropy</i> , kJ/kg·K		
Temp., 7 ℃	Sat. press., <i>P<sub>sat</sub></i> kPa	Sat. Iiquid, <i>v<sub>f</sub></i>	Sat. vapor, <i>v<sub>g</sub></i>	Sat. Iiquid, <i>u<sub>f</sub></i>	Evap., <i>u<sub>fg</sub></i>	Sat. vapor, <i>u<sub>g</sub></i>	Sat. Iiquid, <i>h</i> f	Evap., <i>h<sub>fg</sub></i>	Sat. vapor, <i>h<sub>g</sub></i>	Sat. Iiquid, <i>s<sub>f</sub></i>	Evap., <i>s<sub>fg</sub></i>	Sat. vapor, <i>s<sub>g</sub></i>	
205	1724.3	0.001164	0.11508	872.86	1723.5	2596.4	874.87	1920.0	2794.8	2.3776	4.0154	6.3930	
210	1907.7	0.001173	0.10429	895.38	1702.9	2598.3	897.61	1899.7	2797.3	2.4245	3.9318	6.3563	
215	2105.9	0.001181	0.094680	918.02	1681.9	2599.9	920.50	1878.8	2799.3	2.4712	3.8489	6.3200	
220	2319.6	0.001190	0.086094	940.79	1660.5	2601.3	943.55	1857.4	2801.0	2.5176	3.7664	6.2840	
225	2549.7	0.001199	0.078405	963.70	1638.6	2602.3	966.76	1835.4	2802.2	2.5639	3.6844	6.2483	
230	2797.1	0.001209	0.071505	986.76	1616.1	2602.9	990.14	1812.8	2802.9	2.6100	3.6028	6.2128	
235	3062.6	0.001219	0.065300	1010.0	1593.2	2603.2	1013.7	1789.5	2803.2	2.6560	3.5216	6.1775	
240	3347.0	0.001229	0.059707	1033.4	1569.8	2603.1	1037.5	1765.5	2803.0	2.7018	3.4405	6.1424	
245	3651.2	0.001240	0.054656	1056.9	1545.7	2602.7	1061.5	1740.8	2802.2	2.7476	3.3596	6.1072	
250	3976.2	0.001252	0.050085	1080.7	1521.1	2601.8	1085.7	1715.3	2801.0	2.7933	3.2788	6.0721	
255	4322.9	0.001263	0.045941	1104.7	1495.8	2600.5	1110.1	1689.0	2799.1	2.8390	3.1979	6.0369	
260	4692.3	0.001276	0.042175	1128.8	1469.9	2598.7	1134.8	1661.8	2796.6	2.8847	3.1169	6.0017	
265	5085.3	0.001289	0.038748	1153.3	1443.2	2596.5	1159.8	1633.7	2793.5	2.9304	3.0358	5.9662	
270	5503.0	0.001303	0.035622	1177.9	1415.7	2593.7	1185.1	1604.6	2789.7	2.9762	2.9542	5.9305	
275	5946.4	0.001317	0.032767	1202.9	1387.4	2590.3	1210.7	1574.5	2785.2	3.0221	2.8723	5.8944	
280	6416.6	0.001333	0.030153	1228.2	1358.2	2586.4	1236.7	1543.2	2779.9	3.0681	2.7898	5.8579	
285	6914.6	0.001349	0.027756	1253.7	1328.1	2581.8	1263.1	1510.7	2773.7	3.1144	2.7066	5.8210	
290	7441.8	0.001366	0.025554	1279.7	1296.9	2576.5	1289.8	1476.9	2766.7	3.1608	2.6225	5.7834	
295	7999.0	0.001384	0.023528	1306.0	1264.5	2570.5	1317.1	1441.6	2758.7	3.2076	2.5374	5.7450	
300	8587.9	0.001404	0.021659	1332.7	1230.9	2563.6	1344.8	1404.8	2749.6	3.2548	2.4511	5.7059	
305	9209.4	0.001425	0.019932	1360.0	1195.9	2555.8	1373.1	1366.3	2739.4	3.3024	2.3633	5.6657	
310	9865.0	0.001447	0.018333	1387.7	1159.3	2547.1	1402.0	1325.9	2727.9	3.3506	2.2737	5.6243	
315	10,556	0.001472	0.016849	1416.1	1121.1	2537.2	1431.6	1283.4	2715.0	3.3994	2.1821	5.5816	
320	11,284	0.001499	0.015470	1445.1	1080.9	2526.0	1462.0	1238.5	2700.6	3.4491	2.0881	5.5372	
325	12,051	0.001528	0.014183	1475.0	1038.5	2513.4	1493.4	1191.0	2684.3	3.4998	1.9911	5.4908	
330	12,858	0.001560	0.012979	1505.7	993.5	2499.2	1525.8	1140.3	2666.0	3.5516	1.8906	5.4422	
335	13,707	0.001597	0.011848	1537.5	945.5	2483.0	1559.4	1086.0	2645.4	3.6050	1.7857	5.3907	
340	14,601	0.001638	0.010783	1570.7	893.8	2464.5	1594.6	1027.4	2622.0	3.6602	1.6756	5.3358	
345	15,541	0.001685	0.009772	1605.5	837.7	2443.2	1631.7	963.4	2595.1	3.7179	1.5585	5.2765	
350	16,529	0.001741	0.008806	1642.4	775.9	2418.3	1671.2	892.7	2563.9	3.7788	1.4326	5.2114	
355	17,570	0.001808	0.007872	1682.2	706.4	2388.6	1714.0	812.9	2526.9	3.8442	1.2942	5.1384	
360	18,666	0.001895	0.006950	1726.2	625.7	2351.9	1761.5	720.1	2481.6	3.9165	1.1373	5.0537	
365	19,822	0.002015	0.006009	1777.2	526.4	2303.6	1817.2	605.5	2422.7	4.0004	0.9489	4.9493	
370	21,044	0.002217	0.004953	1844.5	385.6	2230.1	1891.2	443.1	2334.3	4.1119	0.6890	4.8009	
373.95	22,064	0.003106	0.003106	2015.7	0	2015.7	2084.3	0	2084.3	4.4070	0	4.4070	

Source of Data: Tables A–4 through A–8 are generated using the Engineering Equation Solver (EES) software developed by S. A. Klein and F. L. Alvarado. The routine used in calculations is the highly accurate Steam\_IAPWS, which incorporates the 1995 Formulation for the Thermodynamic Properties of Ordinary Water Substance for General and Scientific Use, issued by The International Association for the Properties of Water and Steam (IAPWS). This formulation replaces the 1984 formulation of Haar, Gallagher, and Kell (NBS/NRC Steam Tables, Hemisphere Publishing Co., 1984), which is also available in EES as the routine STEAM. The new formulation is based on the correlations of Saul and Wagner (J. Phys. Chem. Ref. Data, 16, 893, 1987) with modifications to adjust to the International Temperature Scale of 1990. The modifications are described by Wagner and Pruss (J. Phys. Chem. Ref. Data, 22, 783, 1993). The properties of ice are based on Hyland and Wexler, "Formulations for the Thermodynamic Properties of the Saturated Phases of H<sub>2</sub>O from 173.15 K to 473.15 K," *ASHRAE Trans.*, Part 2A, Paper 2793, 1983.

Saturated water—Pressure table

		Specific m	c <i>volume,</i> <sup>3</sup> /kg	Int	ernal ene kJ/kg	rgy,		Enthalpy, kJ/kg			<i>Entropy,</i> kJ/kg·K	
Press., <i>P</i> kPa	Sat. temp., <i>T</i> <sub>sat</sub> ℃	Sat. liquid, v <sub>f</sub>	Sat. vapor, v <sub>g</sub>	Sat. liquid, <i>u<sub>f</sub></i>	Evap., u <sub>fg</sub>	Sat. vapor, u <sub>g</sub>	Sat. liquid, <i>h<sub>f</sub></i>	Evap., h <sub>fg</sub>	Sat. vapor, <i>h<sub>g</sub></i>	Sat. liquid, <i>s<sub>f</sub></i>	Evap., s <sub>fg</sub>	Sat. vapor, <i>s<sub>g</sub></i>
1.0	6.97	0.001000	129.19	29.302	2355.2	2384.5	29.303	2484.4	2513.7	0.1059	8.8690	8.9749
1.5	13.02	0.001001	87.964	54.686	2338.1	2392.8	54.688	2470.1	2524.7	0.1956	8.6314	8.8270
2.0	17.50	0.001001	66.990	73.431	2325.5	2398.9	73.433	2459.5	2532.9	0.2606	8.4621	8.7227
2.5	21.08	0.001002	54.242	88.422	2315.4	2403.8	88.424	2451.0	2539.4	0.3118	8.3302	8.6421
3.0	24.08	0.001003	45.654	100.98	2306.9	2407.9	100.98	2443.9	2544.8	0.3543	8.2222	8.5765
4.0	28.96	0.001004	34.791	121.39	2293.1	2414.5	121.39	2432.3	2553.7	0.4224	8.0510	8.4734
5.0	32.87	0.001005	28.185	137.75	2282.1	2419.8	137.75	2423.0	2560.7	0.4762	7.9176	8.3938
7.5	40.29	0.001008	19.233	168.74	2261.1	2429.8	168.75	2405.3	2574.0	0.5763	7.6738	8.2501
10	45.81	0.001010	14.670	191.79	2245.4	2437.2	191.81	2392.1	2583.9	0.6492	7.4996	8.1488
15	53.97	0.001014	10.020	225.93	2222.1	2448.0	225.94	2372.3	2598.3	0.7549	7.2522	8.0071
20	60.06	0.001017	7.6481	251.40	2204.6	2456.0	251.42	2357.5	2608.9	0.8320	7.0752	7.9073
25	64.96	0.001020	6.2034	271.93	2190.4	2462.4	271.96	2345.5	2617.5	0.8932	6.9370	7.8302
30	69.09	0.001022	5.2287	289.24	2178.5	2467.7	289.27	2335.3	2624.6	0.9441	6.8234	7.7675
40	75.86	0.001026	3.9933	317.58	2158.8	2476.3	317.62	2318.4	2636.1	1.0261	6.6430	7.6691
50	81.32	0.001030	3.2403	340.49	2142.7	2483.2	340.54	2304.7	2645.2	1.0912	6.5019	7.5931
75	91.76	0.001037	2.2172	384.36	2111.8	2496.1	384.44	2278.0	2662.4	1.2132	6.2426	7.4558
100	99.61	0.001043	1.6941	417.40	2088.2	2505.6	417.51	2257.5	2675.0	1.3028	6.0562	7.3589
101.325	99.97	0.001043	1.6734	418.95	2087.0	2506.0	419.06	2256.5	2675.6	1.3069	6.0476	7.3545
125	105.97	0.001048	1.3750	444.23	2068.8	2513.0	444.36	2240.6	2684.9	1.3741	5.9100	7.2841
150	111.35	0.001053	1.1594	466.97	2052.3	2519.2	467.13	2226.0	2693.1	1.4337	5.7894	7.2231
175	116.04	0.001057	1.0037	486.82	2037.7	2524.5	487.01	2213.1	2700.2	1.4850	5.6865	7.1716
200	120.21	0.001061	0.88578	504.50	2024.6	2529.1	504.71	2201.6	2706.3	1.5302	5.5968	7.1270
225	123.97	0.001064	0.79329	520.47	2012.7	2533.2	520.71	2191.0	2711.7	1.5706	5.5171	7.0877
250	127.41	0.001067	0.71873	535.08	2001.8	2536.8	535.35	2181.2	2716.5	1.6072	5.4453	7.0525
275	130.58	0.001070	0.65732	548.57	1991.6	2540.1	548.86	2172.0	2720.9	1.6408	5.3800	7.0207
300	133.52	0.001073	0.60582	561.11	1982.1	2543.2	561.43	2163.5	2724.9	1.6717	5.3200	6.9917
325	136.27	0.001076	0.56199	572.84	1973.1	2545.9	573.19	2155.4	2728.6	1.7005	5.2645	6.9650
350	138.86	0.001079	0.52422	583.89	1964.6	2548.5	584.26	2147.7	2732.0	1.7274	5.2128	6.9402
375	141.30	0.001081	0.49133	594.32	1956.6	2550.9	594.73	2140.4	2735.1	1.7526	5.1645	6.9171
400	143.61	0.001084	0.46242	604.22	1948.9	2553.1	604.66	2133.4	2738.1	1.7765	5.1191	6.8955
450	147.90	0.001088	0.41392	622.65	1934.5	2557.1	623.14	2120.3	2743.4	1.8205	5.0356	6.8561
500	151.83	0.001093	0.37483	639.54	1921.2	2560.7	640.09	2108.0	2748.1	1.8604	4.9603	6.8207
550	155.46	0.001097	0.34261	655.16	1908.8	2563.9	655.77	2096.6	2752.4	1.8970	4.8916	6.7886
600	158.83	0.001101	0.31560	669.72	1897.1	2566.8	670.38	2085.8	2756.2	1.9308	4.8285	6.7593
650	161.98	0.001104	0.29260	683.37	1886.1	2569.4	684.08	2075.5	2759.6	1.9623	4.7699	6.7322
700	164.95	0.001108	0.27278	696.23	1875.6	2571.8	697.00	2065.8	2762.8	1.9918	4.7153	6.7071
750	167.75	0.001111	0.25552	708.40	1865.6	2574.0	709.24	2056.4	2765.7	2.0195	4.6642	6.6837

Saturated water—Pressure table (Concluded)

		<i>Specific</i> m <sup>3</sup> /	<i>volume,</i> kg	Inte	ernal ener kJ/kg	gy,		<i>Enthalpy,</i> kJ/kg			<i>Entropy,</i> kJ/kg·K	
Press.,	Sat. temp., 7 °C	Sat. liquid,	Sat. vapor,	Sat. liquid,	Evap.,	Sat. vapor,	Sat. liquid,	Evap.,	Sat. vapor,	Sat. liquid,	Evap.,	Sat. vapor,
800 850 900 950 1000	170.41 172.94 175.35 177.66 179.88	0.001115 0.001118 0.001121 0.001124 0.001127	vg 0.24035 0.22690 0.21489 0.20411 0.19436	719.97 731.00 741.55 751.67 761.39	1856.1 1846.9 1838.1 1829.6 1821.4	2576.0 2577.9 2579.6 2581.3 2582.8	720.87 731.95 742.56 752.74 762.51	2047.5 2038.8 2030.5 2022.4 2014.6	ng 2768.3 2770.8 2773.0 2775.2 2777.1	2.0457 2.0705 2.0941 2.1166 2.1381	4.6160 4.5705 4.5273 4.4862 4.4470	6.6616 6.6409 6.6213 6.6027 6.5850
1100	184.06	0.001133	0.17745	779.78	1805.7	2585.5	781.03	1999.6	2780.7	2.1785	4.3735	6.5520
1200	187.96	0.001138	0.16326	796.96	1790.9	2587.8	798.33	1985.4	2783.8	2.2159	4.3058	6.5217
1300	191.60	0.001144	0.15119	813.10	1776.8	2589.9	814.59	1971.9	2786.5	2.2508	4.2428	6.4936
1400	195.04	0.001149	0.14078	828.35	1763.4	2591.8	829.96	1958.9	2788.9	2.2835	4.1840	6.4675
1500	198.29	0.001154	0.13171	842.82	1750.6	2593.4	844.55	1946.4	2791.0	2.3143	4.1287	6.4430
1750	205.72	0.001166	0.11344	876.12	1720.6	2596.7	878.16	1917.1	2795.2	2.3844	4.0033	6.3877
2000	212.38	0.001177	0.099587	906.12	1693.0	2599.1	908.47	1889.8	2798.3	2.4467	3.8923	6.3390
2250	218.41	0.001187	0.088717	933.54	1667.3	2600.9	936.21	1864.3	2800.5	2.5029	3.7926	6.2954
2500	223.95	0.001197	0.079952	958.87	1643.2	2602.1	961.87	1840.1	2801.9	2.5542	3.7016	6.2558
3000	233.85	0.001217	0.066667	1004.6	1598.5	2603.2	1008.3	1794.9	2803.2	2.6454	3.5402	6.1856
3500	242.56	0.001235	0.057061	1045.4	1557.6	2603.0	1049.7	1753.0	2802.7	2.7253	3.3991	6.1244
4000	250.35	0.001252	0.049779	1082.4	1519.3	2601.7	1087.4	1713.5	2800.8	2.7966	3.2731	6.0696
5000	263.94	0.001286	0.039448	1148.1	1448.9	2597.0	1154.5	1639.7	2794.2	2.9207	3.0530	5.9737
6000	275.59	0.001319	0.032449	1205.8	1384.1	2589.9	1213.8	1570.9	2784.6	3.0275	2.8627	5.8902
7000	285.83	0.001352	0.027378	1258.0	1323.0	2581.0	1267.5	1505.2	2772.6	3.1220	2.6927	5.8148
8000	295.01	0.001384	0.023525	1306.0	1264.5	2570.5	1317.1	1441.6	2758.7	3.2077	2.5373	5.7450
9000	303.35	0.001418	0.020489	1350.9	1207.6	2558.5	1363.7	1379.3	2742.9	3.2866	2.3925	5.6791
10,000	311.00	0.001452	0.018028	1393.3	1151.8	2545.2	1407.8	1317.6	2725.5	3.3603	2.2556	5.6159
11,000	318.08	0.001488	0.015988	1433.9	1096.6	2530.4	1450.2	1256.1	2706.3	3.4299	2.1245	5.5544
12,000	324.68	0.001526	0.014264	1473.0	1041.3	2514.3	1491.3	1194.1	2685.4	3.4964	1.9975	5.4939
13,000	330.85	0.001566	0.012781	1511.0	985.5	2496.6	1531.4	1131.3	2662.7	3.5606	1.8730	5.4336
14,000	336.67	0.001610	0.011487	1548.4	928.7	2477.1	1571.0	1067.0	2637.9	3.6232	1.7497	5.3728
15,000	342.16	0.001657	0.010341	1585.5	870.3	2455.7	1610.3	1000.5	2610.8	3.6848	1.6261	5.3108
16,000	347.36	0.001710	0.009312	1622.6	809.4	2432.0	1649.9	931.1	2581.0	3.7461	1.5005	5.2466
17,000	352.29	0.001770	0.008374	1660.2	745.1	2405.4	1690.3	857.4	2547.7	3.8082	1.3709	5.1791
18,000	356.99	0.001840	0.007504	1699.1	675.9	2375.0	1732.2	777.8	2510.0	3.8720	1.2343	5.1064
19,000	361.47	0.001926	0.006677	1740.3	598.9	2339.2	1776.8	689.2	2466.0	3.9396	1.0860	5.0256
20,000	365.75	0.002038	0.005862	1785.8	509.0	2294.8	1826.6	585.5	2412.1	4.0146	0.9164	4.9310
21,000	369.83	0.002207	0.004994	1841.6	391.9	2233.5	1888.0	450.4	2338.4	4.1071	0.7005	4.8076
22,000	373.71	0.002703	0.003644	1951.7	140.8	2092.4	2011.1	161.5	2172.6	4.2942	0.2496	4.5439
22,064	373.95	0.003106	0.003106	2015.7	0	2015.7	2084.3	0	2084.3	4.4070	0	4.4070

TABL	E A-6											
Superh	eated wate	r										
Т	V	U.	h	S	V	u	h	S	V	u	h	S
°C	m³/kg	kJ/kg	kJ/kg	kJ/kg∙K	m³/kg	kJ/kg	kJ/kg	kJ/kg∙K	m³/kg	kJ/kg	kJ/kg	kJ/kg∙K
	P =	0.01 MP	a (45.81°	C)*	P =	0.05 MP	a (81.32°	C)	P =	0.10 M	Pa (99.61	.°C)
Sat.†	14.670	2437.2	2583.9	8.1488	3.2403	2483.2	2645.2	7.5931	1.6941	2505.6	2675.0	7.3589
50	14.867	2443.3	2592.0	8.1741								
100	17.196	2515.5	2687.5	8.4489	3.4187	2511.5	2682.4	7.6953	1.6959	2506.2	2675.8	7.3611
150	19.513	2587.9	2783.0	8.6893	3.8897	2585.7	2/80.2	7.9413	1.936/ 2	2582.9	2776.6	7.6148
200	21.020	2736.1	2079.0	9 1015	4.5562	2000.0	2077.0	8 3568	2.1724	2000.2	2073.5	8.0346
300	26.446	2812.3	3076.7	9 2827	5 2841	2811.6	3075.8	8.5387	2.6389	2810.7	3074.5	8 2172
400	31.063	2969.3	3280.0	9.6094	6.2094	2968.9	3279.3	8.8659	3.1027	2968.3	3278.6	8.5452
500	35.680	3132.9	3489.7	9.8998	7.1338	3132.6	3489.3	9.1566	3.5655	3132.2	3488.7	8.8362
600	40.296	3303.3	3706.3	10.1631	8.0577	3303.1	3706.0	9.4201	4.0279	3302.8	3705.6	9.0999
700	44.911	3480.8	3929.9	10.4056	8.9813	3480.6	3929.7	9.6626	4.4900 3	3480.4	3929.4	9.3424
800	49.527	3665.4	4160.6	10.6312	9.9047	3665.2	4160.4	9.8883	4.9519 3	3665.0	4160.2	9.5682
900	54.143	3856.9	4398.3	10.8429	10.8280	3856.8	4398.2	10.1000	5.4137 3	3856.7	4398.0	9.7800
1000	58.758	4055.3	4642.8	11.0429	11.7513	4055.2	4642.7	10.3000	5.8755 4	4055.0	4642.6	9.9800
1200	63.3/3	4260.0	4893.8	11.2320	12.0745	4259.9	4893.7	10.4897	6 7099	4209.8	4893.0	10.1698
1200	72 604	4470.9	5413.4	11.4152	14 5209	4470.8	5413 3	10.8704	7 2605	4470.7	5413.3	10.5504
1000	72.004	0.20 ME	0- (120.2)	11.5057	14.3205	0.20 MP	0 (122 5	20.0420	7.2000 -	0.40 ME	0- (142.6	1000
	P =	0.20 WIP	0706.0	7 1070	P =	0.50 MP	a (155.52	c 0017	P =	0.40 MP	0700.1	1 0)
Sat.	0.885/8	2529.1	2706.3	7.1270	0.60582	2543.2	2724.9	6.9917	0.46242 2	2553.1	2738.1	6.8955
200	1 08049	2654.6	2709.1	7.2010	0.03402	2651.0	2865.9	7 3132	0.470667	2504.4	2752.0	7 1723
250	1.19890	2731.4	2971.2	7.7100	0.79645	2728.9	2967.9	7.5180	0.59520 2	2726.4	2964.5	7.3804
300	1.31623	2808.8	3072.1	7.8941	0.87535	2807.0	3069.6	7.7037	0.65489	2805.1	3067.1	7.5677
400	1.54934	2967.2	3277.0	8.2236	1.03155	2966.0	3275.5	8.0347	0.77265	2964.9	3273.9	7.9003
500	1.78142	3131.4	3487.7	8.5153	1.18672	3130.6	3486.6	8.3271	0.88936 3	3129.8	3485.5	8.1933
600	2.01302	3302.2	3704.8	8.7793	1.34139	3301.6	3704.0	8.5915	1.00558 3	3301.0	3703.3	8.4580
700	2.24434	3479.9	3928.8	9.0221	1.49580	3479.5	3928.2	8.8345	1.12152 3	3479.0	3927.6	8.7012
800	2.47550	3664.7	4159.8	9.2479	1.65004	3664.3	4159.3	9.0605	1.23730 3	3663.9	4158.9	8.9274
900	2.70656	3856.3	4397.7	9.4598	1.80417	3856.0	4397.3	9.2725	1.35298	3855./	4396.9	9.1394
1100	2.95700	4004.0	4042.5	9.0099	2 11226	4054.5 1250 1	4042.0	9.4720	1.400094	4004.0	4041.7	9.5390
1200	3 39938	4470 5	5150.4	10 0304	2 26624	4470.3	5150.2	9.8431	1 69966	4470 2	5150.0	9 7102
1300	3.63026	4687.1	5413.1	10.2029	2.42019	4686.9	5413.0	10.0157	1.81516	4686.7	5412.8	9.8828
	P =	• 0.50 MF	Pa (151.8	3°C)	P =	0.60 MP	a (158.83	3℃)	P =	0.80 MF	Pa (170.4	1°C)
Sat.	0.37483	2560.7	2748.1	6.8207	0.31560	2566.8	2756.2	6.7593	0.24035	2576.0	2768.3	6.6616
200	0.42503	2643.3	2855.8	7.0610	0.35212	2639.4	2850.6	6.9683	0.26088 2	2631.1	2839.8	6.8177
250	0.47443	2723.8	2961.0	7.2725	0.39390	2721.2	2957.6	7.1833	0.29321 2	2715.9	2950.4	7.0402
300	0.52261	2803.3	3064.6	7.4614	0.43442	2801.4	3062.0	7.3740	0.32416 2	2797.5	3056.9	7.2345
350	0.57015	2883.0	3168.1	7.6346	0.47428	2881.6	3166.1	7.5481	0.35442 2	2878.6	3162.2	7.4107
400	0.61/31	2963.7	3272.4	7.7956	0.51374	2962.5	32/0.8	7.7097	0.384292	2960.2	3267.7	7.5/35
600	0.71095	3300.4	3702.5	8 3544	0.59200	3200.2	3483.4	8 2695	0.44332 3	3120.0	3700 1	8 1354
700	0.89696	3478.6	3927.0	8.5978	0.74725	3478.1	3926.4	8.5132	0.56011	3477.2	3925.3	8.3794
800	0.98966	3663.6	4158.4	8.8240	0.82457	3663.2	4157.9	8.7395	0.61820	3662.5	4157.0	8.6061
900	1.08227	3855.4	4396.6	9.0362	0.90179	3855.1	4396.2	8.9518	0.67619 3	3854.5	4395.5	8.8185
1000	1.17480	4054.0	4641.4	9.2364	0.97893	4053.8	4641.1	9.1521	0.73411	4053.3	4640.5	9.0189
1100	1.26728	4259.0	4892.6	9.4263	1.05603	4258.8	4892.4	9.3420	0.79197	4258.3	4891.9	9.2090
1200	1.35972	4470.0	5149.8	9.6071	1.13309	4469.8	5149.6	9.5229	0.84980	4469.4	5149.3	9.3898
1300	1.45214	4686.6	5412.6	9.7797	1.21012	4686.4	5412.5	9.6955	0.90761	4686.1	5412.2	9.5625

\*The temperature in parentheses is the saturation temperature at the specified pressure. † Properties of saturated vapor at the specified pressure.

	TABLI	E A-6											
	Superh	neated wat	er ( <i>Concl</i>	uded)									
1	Т	V	и	h	S	V	и	h	S	v	и	h	S
	°C	m <sup>3</sup> /kg	kJ/kg	kJ/kg	kJ/kg∙K	m <sup>3</sup> /kg	kJ/kg	kJ/kg	kJ/kg∙K	m <sup>3</sup> /kg	kJ/kg	kJ/kg	kJ/kg⋅K
		P =	1.00 MP	a (179.88	°C)	P =	1.20 MP	a (187.96	5°C)	P =	1.40 MPa	(195.04	°C)
	Sat	0 10/27	2502.0	0777 1	6 5950	0 16226	2507.0	2702.0	6 5217	0 14079	2501.9	2700 0	6 4675
	200	0.19437	2002.0	28283	6.5656	0.1603/	2007.0	2705.0	6.5217	0.14078	26027	2803.0	6 4975
	250	0.20002	2710.4	2020.3	6 9265	0.10934	2704.7	2935.6	6.8313	0.14303	2698.9	2927 9	6 7488
	300	0.25799	27937	3051.6	7 1246	0.21386	2789 7	3046.3	7 0335	0.18233	2785.7	3040.9	6 9553
	350	0.28250	2875.7	3158.2	7 3029	0.23455	28727	3154.2	7 2139	0.20029	28697	3150 1	7 1379
	400	0.30661	2957.9	3264.5	7 4670	0.25482	2955.5	3261.3	7 3793	0.21782	2953 1	3258.1	7 3046
	500	0.35411	3125.0	3479.1	7.7642	0.29464	3123.4	3477.0	7.6779	0.25216	3121.8	3474.8	7.6047
	600	0.40111	3297.5	3698.6	8.0311	0.33395	3296.3	3697.0	7.9456	0.28597	3295.1	3695.5	7.8730
	700	0.44783	3476.3	3924.1	8.2755	0.37297	3475.3	3922.9	8.1904	0.31951	3474.4	3921.7	8.1183
	800	0.49438	3661.7	4156.1	8.5024	0.41184	3661.0	4155.2	8.4176	0.35288	3660.3	4154.3	8.3458
	900	0.54083	3853.9	4394.8	8.7150	0.45059	3853.3	4394.0	8.6303	0.38614	3852.7	4393.3	8.5587
	1000	0.58721	4052.7	4640.0	8.9155	0.48928	4052.2	4639.4	8.8310	0.41933	4051.7	4638.8	8.7595
	1100	0.63354	4257.9	4891.4	9.1057	0.52792	4257.5	4891.0	9.0212	0.45247	4257.0	4890.5	8.9497
	1200	0.67983	4469.0	5148.9	9.2866	0.56652	4468.7	5148.5	9.2022	0.48558	4468.3	5148.1	9.1308
	1300	0.72610	4685.8	5411.9	9.4593	0.60509	4685.5	5411.6	9.3750	0.51866	4685.1	5411.3	9.3036
		P =	1.60 MPa	a (201.37°	°C)	P =	1.80 MP	Pa (207.1	1°C)	P =	2.00 MPa	(212.38	°C)
	Sat.	0.12374	2594.8	2792.8	6.4200	0.11037	2597.3	2795.9	6.3775	0.09959	2599.1	2798.3	6.3390
	225	0.13293	2645.1	2857.8	6.5537	0.11678	2637.0	2847.2	6.4825	0.10381	2628.5	2836.1	6.4160
	250	0.14190	2692.9	2919.9	6.6753	0.12502	2686.7	2911.7	6.6088	0.11150	2680.3	2903.3	6.5475
	300	0.15866	2781.6	3035.4	6.8864	0.14025	2777.4	3029.9	6.8246	0.12551	2773.2	3024.2	6.7684
	350	0.17459	2866.6	3146.0	7.0713	0.15460	2863.6	3141.9	7.0120	0.13860	2860.5	3137.7	6.9583
	400	0.19007	2950.8	3254.9	7.2394	0.16849	2948.3	3251.6	7.1814	0.15122	2945.9	3248.4	7.1292
	500	0.22029	3120.1	3472.6	7.5410	0.19551	3118.5	3470.4	7.4845	0.17568	3116.9	3468.3	7.4337
	600	0.24999	3293.9	3693.9	7.8101	0.22200	3292.7	3692.3	7.7543	0.19962	3291.5	3690.7	7.7043
	700	0.27941	3473.5	3920.5	8.0558	0.24822	3472.6	3919.4	8.0005	0.22326	3471.7	3918.2	7.9509
	800	0.30865	3659.5	4153.4	8.2834	0.27426	3658.8	4152.4	8.2284	0.24674	3658.0	4151.5	8.1791
	900	0.33780	3852.1	4392.6	8.4965	0.30020	3851.5	4391.9	8.4417	0.27012	3850.9	4391.1	8.3925
	1000	0.36687	4051.2	4638.2	8.6974	0.32606	4050.7	4637.6	8.6427	0.29342	4050.2	4637.1	8.5936
	1100	0.39589	4256.6	4890.0	8.8878	0.35188	4256.2	4889.6	8.8331	0.31667	4255.7	4889.1	8.7842
	1200	0.42488	4467.9	5147.7	9.0689	0.37766	4467.6	5147.3	9.0143	0.33989	4467.2	5147.0	8.9654
	1300	0.45383	4684.8	5410.9	9.2418	0.40341	4684.5	5410.6	9.1872	0.36308	4684.2	5410.3	9.1384
		P =	2.50 MP	a (223.95	°C)	P =	3.00 MP	a (233.85	i°C)	P =	3.50 MPa	(242.56	°C)
	Sat.	0.07995	2602.1	2801.9	6.2558	0.06667	2603.2	2803.2	6.1856	0.05706	2603.0	2802.7	6.1244
	225	0.08026	2604.8	2805.5	6.2629	0 07000		0050 5	c	0.05076			C 17C1
	250	0.08/05	2663.3	2880.9	6.4107	0.07063	2644.7	2856.5	6.2893	0.05876	2624.0	2829.7	6.1764
	300	0.09894	2762.2	3009.6	6.6459	0.08118	2/50.8	2994.3	6.5412	0.06845	2/38.8	2978.4	6.4484
	350	0.10979	2852.5	3127.0	6.8424	0.09056	2844.4	3116.1	6.7450	0.07680	2836.0	3104.9	6.6601
	400	0.12012	2939.8	3240.1	7.0170	0.09938	2933.6	3231.7	0.9235	0.08456	2927.2	3223.2	6.8428
	400	0.13010	2112.0	2462.0	7.2254	0.10789	2109.6	2457.2	7.0000	0.09198	2104 5	2451 7	7.0074
	600	0.15999	2200 E	2606.0	7.5204	0.11020	2205 5	2602 0	7.2309	0.09919	2202 5	2679.0	7.1095
	700	0.10931	3200.0	2015.2	7.09/9	0.13245	3263.0	2012.0	7.5105	0.11325	3262.3	2000.2	7.4337
	800	0.17655	3656.2	A149.2	8 0744	0.14641	3654.2	4146.0	7 9885	0.12702	3652 5	4144.6	7.0000
	900	0.21507	3849.4	4149.2	8 2882	0.17988	38/17 0	4140.9	8 2028	0.15410	38/6 /	4144.0	8 1304
	1000	0.23466	4049.0	4635.6	8 4897	0.19549	4047.7	4634.2	8 4045	0.16751	4046.4	4632.7	8 3324
	1100	0.25330	4254.7	4035.0	8 6804	0.21105	4047.7	4034.2	8 5955	0.18087	4040.4	4032.7	8 5236
	1200	0.23330	1166.2	51/6.0	8 8619	0.22659	4255.0	5145 1	8 7771	0.10420	4252.5	5144 1	8 7052
	1300	0.29048	4683.4	5409.5	9.0349	0.24207	4682.6	5408.8	8.9502	0.20750	4681.8	5408.0	8.8786
	1000	5.25040		0.00.0	5.00-15	012 1201	.002.0	0.00.0	3.3002	0.20700		0.00.0	5.07.00

TABL	E A-6											
Superh	neated water (	(Contir	nued)									
Т	v u		h	S	V	и	h	S	v	и	h	S
°C	m <sup>3</sup> /kg kJ	l/kg	kJ/kg	kJ/kg∙K	m <sup>3</sup> /kg	kJ/kg	kJ/kg	kJ/kg∙K	m <sup>3</sup> /kg	kJ/kg	kJ/kg	kJ/kg∙K
	<i>P</i> = 4	I.O MPa	(250.35	°C)	P =	= 4.5 MPa	(257.44%	C)	P =	5.0 MPa	(263.94°	C)
Sat.	0.04978 26	601.7	2800.8	6.0696	0.04406	2599.7	2798.0	6.0198	0.03945	2597.0	2794.2	5.9737
275	0.05461 26	668.9	2887.3	6.2312	0.04733	2651.4	2864.4	6.1429	0.04144	2632.3	2839.5	6.0571
300	0.05887 27	726.2	2961.7	6.3639	0.05138	2713.0	2944.2	6.2854	0.04535	2699.0	2925.7	6.2111
350	0.06647 28	327.4	3093.3	6.5843	0.05842	2818.6	3081.5	6.5153	0.05197	2809.5	3069.3	6.4516
400	0.07343 29	920.8	3214.5	6.0296	0.06477	2914.2	3205.7	6.7071	0.05784	2907.5	3196.7	6.0210
400 500	0.08644 31	100.3	3446.0	7 0922	0.07076	3005.6	344.2	7 0323	0.00552	3000.0	3/3/ 7	6.0210
600	0.09886 32	279.4	3674.9	7.3706	0.08766	3276.4	3670.9	7.3127	0.07870	3273.3	3666.9	7.2605
700	0.11098 34	462.4	3906.3	7.6214	0.09850	3460.0	3903.3	7.5647	0.08852	3457.7	3900.3	7.5136
800	0.12292 36	650.6	4142.3	7.8523	0.10916	3648.8	4140.0	7.7962	0.09816	3646.9	4137.7	7.7458
900	0.13476 38	844.8	4383.9	8.0675	0.11972	3843.3	4382.1	8.0118	0.10769	3841.8	4380.2	7.9619
1000	0.14653 40	045.1	4631.2	8.2698	0.13020	4043.9	4629.8	8.2144	0.11715	4042.6	4628.3	8.1648
1100	0.15824 42	251.4	4884.4	8.4612	0.14064	4250.4	4883.2	8.4060	0.12655	4249.3	4882.1	8.3566
1200	0.16992 44	463.5	5143.2	8.6430	0.15103	4462.6	5142.2	8.5880	0.13592	4461.6	5141.3	8.5388
1300	0.18157 46	580.9	5407.2	8.8164	0.16140	4680.1	5406.5	8.7616	0.14527	4679.3	5405.7	8.7124
	P = 6	.0 MPa	(275.59°	C)	P =	= 7.0 MPa	(285.83°	C)	P =	8.0 MPa	(295.01	°C)
Sat.	0.03245 25	589.9	2784.6	5.8902	0.027378	2581.0	2772.6	5.8148	0.023525	2570.5	2758.7	5.7450
300	0.03619 26	668.4	2885.6	6.0703	0.029492	2633.5	2839.9	5.9337	0.024279	2592.3	2786.5	5.7937
350	0.04225 27	790.4	3043.9	6.3357	0.035262	2770.1	3016.9	6.2305	0.029975	2748.3	2988.1	6.1321
400	0.04742 28	893.7	3178.3	6.5432	0.039958	2879.5	3159.2	6.4502	0.034344	2864.6	3139.4	6.3658
450	0.05217 29	989.9	3302.9	6.7219	0.044187	2979.0	3288.3	6.6353	0.038194	2967.8	3273.3	6.5579
500	0.05667 30	J83.1 175.2	3423.1	0.8820	0.048157	30/4.3	3411.4 2521.6	6.8000	0.041/6/	3065.4	3399.0	6.9900
600	0.06527 32	267.2	3658.8	7.0508	0.051900	3261.0	3650.6	7 0910	0.045172	3254.7	3642.4	7 0221
700	0.07355 34	453.0	3894.3	7.4247	0.062850	3448.3	3888.3	7.3487	0.054829	3443.6	3882.2	7.2822
800	0.08165 36	643.2	4133.1	7.6582	0.069856	3639.5	4128.5	7.5836	0.061011	3635.7	4123.8	7.5185
900	0.08964 38	838.8	4376.6	7.8751	0.076750	3835.7	4373.0	7.8014	0.067082	3832.7	4369.3	7.7372
1000	0.09756 40	040.1	4625.4	8.0786	0.083571	4037.5	4622.5	8.0055	0.073079	4035.0	4619.6	7.9419
1100	0.10543 42	247.1	4879.7	8.2709	0.090341	4245.0	4877.4	8.1982	0.079025	4242.8	4875.0	8.1350
1200	0.11326 44	459.8	5139.4	8.4534	0.097075	4457.9	5137.4	8.3810	0.084934	4456.1	5135.5	8.3181
1300	0.12107 46	677.7	5404.1	8.6273	0.103781	4676.1	5402.6	8.5551	0.090817	4674.5	5401.0	8.4925
	P = 9.	.0 MPa	(303.35°	C)	P =	10.0 MP	a (311.00°	°C)	P =	12.5 MPa	(327.81	°C)
Sat.	0.020489 25	558.5	2742.9	5.6791	0.018028	2545.2	2725.5	5.6159	0.013496	2505.6	2674.3	5.4638
325	0.023284 26	647.6	2857.1	5.8738	0.019877	2611.6	2810.3	5.7596				= =1.00
350	0.025816 27	725.0	2957.3	6.0380	0.022440	2699.6	2924.0	5.9460	0.016138	2624.9	2826.6	5.7130
400	0.029960 28	549.2 056.2	3118.8	6.28/6	0.026436	2833.1	3097.5	6.2141	0.020030	2/89.6	3040.0	6.0433
400 500	0.035524 29	156.3	3230.0	6 6603	0.029782	2944.5	3242.4	6 5005	0.025019	2913.7	3201.5	6.4651
550	0.039885 31	153.0	3512.0	6.8164	0.035655	3145.4	3502.0	6.7585	0.028033	3126.1	3476.5	6.6317
600	0.042861 32	248.4	3634.1	6.9605	0.038378	3242.0	3625.8	6.9045	0.030306	3225.8	3604.6	6.7828
650	0.045755 33	343.4	3755.2	7.0954	0.041018	3338.0	3748.1	7.0408	0.032491	3324.1	3730.2	6.9227
700	0.048589 34	438.8	3876.1	7.2229	0.043597	3434.0	3870.0	7.1693	0.034612	3422.0	3854.6	7.0540
800	0.054132 36	632.0	4119.2	7.4606	0.048629	3628.2	4114.5	7.4085	0.038724	3618.8	4102.8	7.2967
900	0.059562 38	829.6	4365.7	7.6802	0.053547	3826.5	4362.0	7.6290	0.042720	3818.9	4352.9	7.5195
1000	0.064919 40	032.4	4616.7	7.8855	0.058391	4029.9	4613.8	7.8349	0.046641	4023.5	4606.5	7.7269
1100	0.070224 42	240.7	4872.7	8.0791	0.063183	4238.5	4870.3	8.0289	0.050510	4233.1	4864.5	7.9220
1200	0.075492 44	454.2 672 9	5133.6	8.2625	0.067938	4452.4	5131.7 5398.0	8.2126	0.054342	4447.7	5127.0	8.1065
1000	0.00070040	572.5	5555.5	0.40/1	0.072007	10/1.0	5550.0	0.0074	0.00014/	1007.5	5554.1	0.2015

TABL	E A-6											
Super	heated wate	r ( <i>Conclu</i>	ıded)									
T	V	11	h	s	V	11	h	s	V	11	h	s
°C	m <sup>3</sup> /kg	kJ/kg	kJ/kg	kJ/kg∙K	m <sup>3</sup> /kg	kJ/kg	kJ/kg	kJ/kg⋅K	m <sup>3</sup> /kg	kJ/kg	 kJ/kg	kJ/kg∙K
	P =	15.0 MP	(342.16	(3)	P = 1	17.5 MPa	(354.67	(	P =	20.0 MPz	(365.75	
Sat	0.010241	2455.7	2610.9	5 2109	0.007022	2200 7	2520.5	5 1425	0.005962	220.0 10 0	2412 1	4 0210
350	0.010341	2455.7	2693.1	5.3108	0.007932	2390.7	2029.0	5.1455	0.005862	2294.8	2412.1	4.9310
400	0.015671	2740.6	2975.7	5.8819	0.012463	2684.3	2902.4	5.7211	0.009950	2617.9	2816.9	5.5526
450	0.018477	2880.8	3157.9	6.1434	0.015204	2845.4	3111.4	6.0212	0.012721	2807.3	3061.7	5.9043
500	0.020828	2998.4	3310.8	6.3480	0.017385	2972.4	3276.7	6.2424	0.014793	2945.3	3241.2	6.1446
550	0.022945	3106.2	3450.4	6.5230	0.019305	3085.8	3423.6	6.4266	0.016571	3064.7	3396.2	6.3390
600	0.024921	3209.3	3583.1	6.6796	0.021073	3192.5	3561.3	6.5890	0.018185	3175.3	3539.0	6.5075
650	0.026804	3310.1	3712.1	6.8233	0.022742	3295.8	3693.8	6.7366	0.019695	3281.4	3675.3	6.6593
700	0.028621	3409.8	3839.1	6.9573	0.024342	3397.5	3823.5	6.8735	0.021134	3385.1	3807.8	6.7991
800	0.032121	3609.3	4091.1	7.2037	0.027405	3599.7	4079.3	7.1237	0.023870	3590.1	4067.5	7.0531
900	0.035503	3811.2	4343.7	7.4288	0.030348	3803.5	4334.6	7.3511	0.026484	3/95./	4325.4	7.2829
11000	0.038808	4017.1	4599.2	7.03/8	0.033215	4010.7	4592.0	7.5010	0.029020	4004.3	4584.7	7.4950
1200	0.042062	4227.7	4000.0	7.0009 8.0102	0.036029	4222.3	400Z.0	7.7000	0.031504	4210.9	4047.0 5112.0	7.0933
1200	0.043279	4445.1	5390.3	8 1952	0.038806	4450.5	5386.5	8 1215	0.035952	4455.0	5382.7	8 0574
1000	0.040405	4000.0	0.000	0.1552	0.041000	+0000.2		0.1210	0.000071	4000.2	0002.7	0.0074
		P = 25	.0 MPa			P = 30.0	ј мра			P = 35.		
375	0.001978	1799.9	1849.4	4.0345	0.001792	1738.1	1791.9	3.9313	0.001701	1702.8	1762.4	3.8724
400	0.006005	2428.5	25/8./	5.1400	0.002798	2068.9	2152.8	4.4/58	0.002105	1914.9	1988.6	4.2144
425	0.007886	2007.8	2805.0	5.4708	0.005299	2452.9	2011.8	5.14/3	0.003434	2203.3	2373.5	4.//51
500	0.009170	2887.3	2950.0	5 9643	0.008691	2824.0	3084.8	5 7956	0.004937	2497.0	2071.0	5 6331
550	0.012736	3020.8	3339.2	6.1816	0.010175	2974.5	3279.7	6.0403	0.008348	2925.8	3218.0	5.9093
600	0.014140	3140.0	3493.5	6.3637	0.011445	3103.4	3446.8	6.2373	0.009523	3065.6	3399.0	6.1229
650	0.015430	3251.9	3637.7	6.5243	0.012590	3221.7	3599.4	6.4074	0.010565	3190.9	3560.7	6.3030
700	0.016643	3359.9	3776.0	6.6702	0.013654	3334.3	3743.9	6.5599	0.011523	3308.3	3711.6	6.4623
800	0.018922	3570.7	4043.8	6.9322	0.015628	3551.2	4020.0	6.8301	0.013278	3531.6	3996.3	6.7409
900	0.021075	3780.2	4307.1	7.1668	0.017473	3764.6	4288.8	7.0695	0.014904	3749.0	4270.6	6.9853
1000	0.023150	3991.5	4570.2	7.3821	0.019240	3978.6	4555.8	7.2880	0.016450	3965.8	4541.5	7.2069
1100	0.025172	4206.1	4835.4	7.5825	0.020954	4195.2	4823.9	7.4906	0.017942	4184.4	4812.4	7.4118
1200	0.027157	4424.6	5103.5	7.7710	0.022630	4415.3	5094.2	7.6807	0.019398	4406.1	5085.0	7.6034
1300	0.029115	4647.2	5375.1	7.9494	0.024279	4639.2	5367.6	7.8602	0.020827	4631.2	5360.2	7.7841
		P = 40.	0 MPa			P = 50.0	O MPa			P = 60.	0 MPa	
375	0.001641	1677.0	1742.6	3.8290	0.001560	1638.6	1716.6	3.7642	0.001503	1609.7	1699.9	3.7149
400	0.001911	1855.0	1931.4	4.1145	0.001731	1787.8	1874.4	4.0029	0.001633	1745.2	1843.2	3.9317
425	0.002538	2097.5	2199.0	4.5044	0.002009	1960.3	2060.7	4.2746	0.001816	1892.9	2001.8	4.1630
450	0.003692	2364.2	2511.8	4.9449	0.002487	2160.3	2284.7	4.5896	0.002086	2055.1	2180.2	4.4140
500	0.005623	2681.6	2906.5	5.4744	0.003890	2528.1	2722.6	5.1762	0.002952	2393.2	2570.3	4.9356
550	0.006985	28/5.1	3154.4	5./85/	0.005118	2/69.5	3025.4	5.5563	0.003955	2664.6	2901.9	5.3517
600	0.008089	3020.8	3300.4	6.0170	0.006108	2947.1	3232.0	5.8245	0.004833	2000.0	3100.8	5.0527
700	0.009053	3282.0	3679.2	6 3740	0.008957	3228 7	3614.6	6 2179	0.005591	3175.4	3551.2	6.0814
800	0.009930	3511.8	3972.6	6 6613	0.009073	3472.2	3925.8	6 5225	0.000205	3432.6	3880.0	6 4033
900	0.012980	3733.3	4252.5	6.9107	0.010296	3702.0	4216.8	6.7819	0.008519	3670.9	4182.1	6.6725
1000	0.014360	3952.9	4527.3	7.1355	0.011441	3927.4	4499.4	7.0131	0.009504	3902.0	4472.2	6.9099
1100	0.015686	4173.7	4801.1	7.3425	0.012534	4152.2	4778.9	7.2244	0.010439	4130.9	4757.3	7.1255
1200	0.016976	4396.9	5075.9	7.5357	0.013590	4378.6	5058.1	7.4207	0.011339	4360.5	5040.8	7.3248
1300	0.018239	4623.3	5352.8	7.7175	0.014620	4607.5	5338.5	7.6048	0.012213	4591.8	5324.5	7.5111

TABL	E A-7											
Comp	ressed liqui	d water										
Т	V	и	h	s	v	и	h	s	V	и	h	s
°C	m³/kg	kJ/kg	kJ/kg	kJ/kg∙K	m <sup>3</sup> /kg	kJ/kg	kJ/kg	kJ/kg∙K	m <sup>3</sup> /kg	kJ/kg	kJ/kg	kJ/kg∙K
	P =	= 5 MPa	(263.94°C	;)	P =	10 MPa	(311.00°C	)	P =	15 MPa	(342.16°	C)
Sat.	0.0012862	1148.1	1154.5	2.9207	0.0014522	1393.3	1407.9	3.3603	0.0016572	1585.5	1610.3	3.6848
0	0.0009977	0.04	5.03	0.0001	0.0009952	0.12	10.07	0.0003	0.0009928	0.18	15.07	0.0004
20	0.0009996	83.61	88.61	0.2954	0.0009973	83.31	93.28	0.2943	0.0009951	83.01	97.93	0.2932
40	0.0010057	166.92	171.95	0.5705	0.0010035	166.33	176.37	0.5685	0.0010013	165.75	180.77	0.5666
80	0.0010149	250.29	200.30	0.8287	0.0010127	249.43	209.00	0.8260	0.0010105	248.58	203.74	1.0650
100	0.0010287	JJJJ.02	122 85	1.0723	0.0010244	116.23	342.94 126.62	1.0091	0.0010221	JJ1.39	340.92 430.30	1.0009
120	0.0010410	501 91	507 19	1.5034	0.0010585	500 18	420.02 510.73	1.2990	0.0010501	414.65	514 28	1.2950
140	0.0010769	586.80	592.18	1.7344	0.0010738	584.72	595.45	1.7293	0.0010708	582.69	598.75	1.7243
160	0.0010988	672.55	678.04	1.9374	0.0010954	670.06	681.01	1.9316	0.0010920	667.63	684.01	1.9259
180	0.0011240	759.47	765.09	2.1338	0.0011200	756.48	767.68	2.1271	0.0011160	753.58	770.32	2.1206
200	0.0011531	847.92	853.68	2.3251	0.0011482	844.32	855.80	2.3174	0.0011435	840.84	858.00	2.3100
220	0.0011868	938.39	944.32	2.5127	0.0011809	934.01	945.82	2.5037	0.0011752	929.81	947.43	2.4951
240	0.0012268	1031.6	1037.7	2.6983	0.0012192	1026.2	1038.3	2.6876	0.0012121	1021.0	1039.2	2.6774
260	0.0012755	1128.5	1134.9	2.8841	0.0012653	1121.6	1134.3	2.8710	0.0012560	1115.1	1134.0	2.8586
280					0.0013226	1221.8	1235.0	3.0565	0.0013096	1213.4	1233.0	3.0410
300					0.0013980	1329.4	1343.3	3.2488	0.0013783	1317.6	1338.3	3.2279
320									0.0014733	1431.9	1454.0	3.4263
340									0.0016311	1567.9	1592.4	3.6555
	P =	20 MPa	(365.75°(	C)		<i>P</i> = 30	MPa			P = 50	) MPa	
Sat.	0.0020378	1785.8	1826.6	4.0146								
0	0.0009904	0.23	20.03	0.0005	0.0009857	0.29	29.86	0.0003	0.0009767	0.29	49.13	-0.0010
20	0.0009929	82.71	102.57	0.2921	0.0009886	82.11	111.77	0.2897	0.0009805	80.93	129.95	0.2845
40	0.0009992	165.17	185.16	0.5646	0.0009951	164.05	193.90	0.5607	0.0009872	161.90	211.25	0.5528
60	0.0010084	247.75	267.92	0.8208	0.0010042	246.14	276.26	0.8156	0.0009962	243.08	292.88	0.8055
80	0.0010199	330.50	350.90	1.0627	0.0010155	328.40	358.86	1.0564	0.0010072	324.42	374.78	1.0442
100	0.0010337	413.50	434.17	1.2920	0.0010290	410.87	441.74	1.2847	0.0010201	405.94	456.94	1.2705
120	0.0010496	496.85	517.84	1.5105	0.0010445	493.66	525.00	1.5020	0.0010349	487.69	539.43	1.4859
140	0.0010679	580.71	602.07	1.7194	0.0010623	5/6.90	608.76	1.7098	0.0010517	269.77	022.30 705.95	1.0910
190	0.0010880	750 79	772.02	2 11/2	0.0010823	745.40	779 55	2 1020	0.0010704	725.40	700.00	2.0700
200	0.0011122	837 / 9	860.27	2.1143	0.0011049	831 11	865.02	2.1020	0.0010914	819.45	875.19	2.0790
220	0.0011697	925.77	949 16	2.3027	0.0011504	918 15	952.93	2.2000	0.0011412	904 39	961.45	2.2020
240	0.0012053	1016.1	1040.2	2.6676	0.0011927	1006.9	1042.7	2.6491	0.0011708	990.55	1049.1	2.6156
260	0.0012472	1109.0	1134.0	2.8469	0.0012314	1097.8	1134.7	2.8250	0.0012044	1078.2	1138.4	2.7864
280	0.0012978	1205.6	1231.5	3.0265	0.0012770	1191.5	1229.8	3.0001	0.0012430	1167.7	1229.9	2.9547
300	0.0013611	1307.2	1334.4	3.2091	0.0013322	1288.9	1328.9	3.1761	0.0012879	1259.6	1324.0	3.1218
320	0.0014450	1416.6	1445.5	3.3996	0.0014014	1391.7	1433.7	3.3558	0.0013409	1354.3	1421.4	3.2888
340	0.0015693	1540.2	1571.6	3.6086	0.0014932	1502.4	1547.1	3.5438	0.0014049	1452.9	1523.1	3.4575
360	0.0018248	1703.6	1740.1	3.8787	0.0016276	1626.8	1675.6	3.7499	0.0014848	1556.5	1630.7	3.6301
380					0.0018729	1782.0	1838.2	4.0026	0.0015884	1667.1	1746.5	3.8102

TABLE	A-8											
Saturate	ed ice-wat	er vapor										
		<i>Specifi</i> m	<i>c volume,</i> <sup>3</sup> /kg	<i>I</i>	nternal er kJ/kg	nergy,		<i>Enthalpy</i> kJ/kg	(,		E <i>ntropy,</i> kJ/kg·K	
	Sat.	Sat.	Sat.	Sat.		Sat.	Sat.		Sat.	Sat.		Sat.
Temp.,	press.,	ice,	vapor,	ice,	Subl.,	vapor,	ice,	Subl.,	vapor,	ice,	Subl.,	vapor,
T ℃	P <sub>sat</sub> kPa	Vi	Vg	U <sub>i</sub>	Uig	Ug	h <sub>i</sub>	h <sub>ig</sub>	hg	s <sub>i</sub>	S <sub>ig</sub>	Sg
0.01	0.61169	0.001091	205.99	-333.40	2707.9	2374.5	-333.40	2833.9	2500.5	-1.2202	10.374	9.154
0	0.61115	0.001091	206.17	-333.43	2707.9	2374.5	-333.43	2833.9	2500.5	-1.2204	10.375	9.154
-2	0.51772	0.001091	241.62	-337.63	2709.4	2371.8	-337.63	2834.5	2496.8	-1.2358	10.453	9.218
-4	0.43748	0.001090	283.84	-341.80	2710.8	2369.0	-341.80	2835.0	2493.2	-1.2513	10.533	9.282
-6	0.36873	0.001090	334.27	-345.94	2712.2	2366.2	-345.93	2835.4	2489.5	-1.2667	10.613	9.347
-8	0.30998	0.001090	394.66	-350.04	2713.5	2363.5	-350.04	2835.8	2485.8	-1.2821	10.695	9.413
-10	0.25990	0.001089	467.17	-354.12	2714.8	2360.7	-354.12	2836.2	2482.1	-1.2976	10.778	9.480
-12	0.21732	0.001089	554.47	-358.17	2716.1	2357.9	-358.17	2836.6	2478.4	-1.3130	10.862	9.549
-14	0.18121	0.001088	659.88	-362.18	2717.3	2355.2	-362.18	2836.9	2474.7	-1.3284	10.947	9.618
-16	0.15068	0.001088	787.51	-366.17	2718.6	2352.4	-366.17	2837.2	2471.0	-1.3439	11.033	9.689
-18	0.12492	0.001088	942.51	-370.13	2719.7	2349.6	-370.13	2837.5	2467.3	-1.3593	11.121	9.761
-20	0.10326	0.001087	1131.3	-374.06	2720.9	2346.8	-374.06	2837.7	2463.6	-1.3748	11.209	9.835
-22	0.08510	0.001087	1362.0	-377.95	2722.0	2344.1	-377.95	2837.9	2459.9	-1.3903	11.300	9.909
-24	0.06991	0.001087	1644.7	-381.82	2723.1	2341.3	-381.82	2838.1	2456.2	-1.4057	11.391	9.985
-26	0.05725	0.001087	1992.2	-385.66	2724.2	2338.5	-385.66	2838.2	2452.5	-1.4212	11.484	10.063
-28	0.04673	0.001086	2421.0	-389.47	2725.2	2335.7	-389.47	2838.3	2448.8	-1.4367	11.578	10.141
-30	0.03802	0.001086	2951.7	-393.25	2726.2	2332.9	-393.25	2838.4	2445.1	-1.4521	11.673	10.221
-32	0.03082	0.001086	3610.9	-397.00	2727.2	2330.2	-397.00	2838.4	2441.4	-1.4676	11.770	10.303
-34	0.02490	0.001085	4432.4	-400.72	2728.1	2327.4	-400.72	2838.5	2437.7	-1.4831	11.869	10.386
-36	0.02004	0.001085	5460.1	-404.40	2729.0	2324.6	-404.40	2838.4	2434.0	-1.4986	11.969	10.470
-38	0.01608	0.001085	6750.5	-408.07	2729.9	2321.8	-408.07	2838.4	2430.3	-1.5141	12.071	10.557
-40	0.01285	0.001084	8376.7	-411.70	2730.7	2319.0	-411.70	2838.3	2426.6	-1.5296	12.174	10.644

TABL	TABLE A-11												
Satura	ted refrige	rant-134a	Temperatur	e table									
		<i>Specific</i> m <sup>3</sup> /l	<i>volume,</i> kg	Inte	<i>rnal ener</i> kJ/kg	gy,		E <i>nthalpy,</i> kJ/kg			<i>Entropy,</i> kJ/kg·K		
Temp	Sat. press	Sat. liquid.	Sat. vapor.	Sat. liquid.	Evap	Sat. vapor.	Sat. liquid.	Evap	Sat. vapor.	Sat. liquid.	Evap	Sat. vapor.	
T°C	P <sub>sat</sub> kPa	V <sub>f</sub>	V <sub>g</sub>	U <sub>f</sub>	U <sub>fg</sub>	u <sub>g</sub>	h <sub>f</sub>	h <sub>fg</sub>	h <sub>g</sub>	S <sub>f</sub>	S <sub>fg</sub>	S <sub>g</sub>	
-40	51.25	0.0007053	0.36064	-0.036	207.42	207.38	0.00	225.86	225.86	0.00000	0.96869	0.96869	
-38	56.86	0.0007082	0.32718	2.472	206.06	208.53	2.512	224.62	227.13	0.010/1	0.95516	0.96588	
-36	62.95	0.000/111	0.29740	4.987	204.69	209.68	5.032	223.37	228.40	0.02137	0.94182	0.96319	
-34	69.56	0.0007141	0.27082	7.509	203.32	210.83	7.559	222.10	229.66	0.03196	0.92867	0.96063	
-32	76.71	0.0007171	0.24706	10.04	201.94	211.97	10.09	220.83	230.93	0.04249	0.91569	0.95819	
-30	84.43	0.0007201	0.22577	12.58	200.55	213.12	12.64	219.55	232.19	0.05297	0.90289	0.95586	
-28	92.76	0.0007232	0.20666	15.12	199.15	214.27	15.19	218.25	233.44	0.06339	0.89024	0.95364	
-26	101.73	0.0007264	0.18947	17.67	197.75	215.42	17.75	216.95	234.70	0.07376	0.87776	0.95152	
-24	111.37	0.0007296	0.17398	20.23	196.34	216.57	20.31	215.63	235.94	0.08408	0.86542	0.94950	
-22	121.72	0.0007328	0.15999	22.80	194.92	217.71	22.89	214.30	237.19	0.09435	0.85323	0.94758	
-20	132.82	0.0007361	0.14735	25.37	193.49	218.86	25.47	212.96	238.43	0.10456	0.84119	0.94575	
-18	144.69	0.0007394	0.13589	27.96	192.05	220.00	28.07	211.60	239.67	0.11473	0.82927	0.94401	
-16	157.38	0.0007428	0.12550	30.55	190.60	221.15	30.67	210.23	240.90	0.12486	0.81749	0.94234	
-14	170.93	0.0007463	0.11605	33.15	189.14	222.29	33.28	208.84	242.12	0.13493	0.80583	0.94076	
-12	185.37	0.0007498	0.10744	35.76	187.66	223.42	35.90	207.44	243.34	0.14497	0.79429	0.93925	
-10	200.74	0.0007533	0.099600	38.38	186.18	224.56	38.53	206.02	244.55	0.15496	0.78286	0.93782	
-8	217.08	0.0007570	0.092438	41.01	184.69	225.69	41.17	204.59	245.76	0.16491	0.77154	0.93645	
-6	234.44	0.0007607	0.085888	43.64	183.18	226.82	43.82	203.14	246.95	0.17482	0.76033	0.93514	
-4	252.85	0.0007644	0.079889	46.29	181.66	227.94	46.48	201.66	248.14	0.18469	0.74921	0.93390	
-2	272.36	0.0007683	0.074388	48.94	180.12	229.07	49.15	200.17	249.33	0.19452	0.73819	0.93271	
0	293.01	0.0007722	0.069335	51.61	178.58	230.18	51.83	198.67	250.50	0.20432	0.72726	0.93158	
2	314.84	0.0007761	0.064690	54.28	177.01	231.30	54.53	197.14	251.66	0.21408	0.71641	0.93050	
4	337.90	0.0007802	0.060412	56.97	175.44	232.40	57.23	195.58	252.82	0.22381	0.70565	0.92946	
6	362.23	0.0007843	0.056469	59.66	173.84	233.51	59.95	194.01	253.96	0.23351	0.69496	0.92847	
8	387.88	0.0007886	0.052829	62.37	172.23	234.60	62.68	192.42	255.09	0.24318	0.68435	0.92752	
10	414.89	0.0007929	0.049466	65.09	170.61	235.69	65.42	190.80	256.22	0.25282	0.67380	0.92661	
12	443.31	0.0007973	0.046354	67.82	168.96	236.78	68.17	189.16	257.33	0.26243	0.66331	0.92574	
14	473.19	0.0008018	0.043471	70.56	167.30	237.86	70.94	187.49	258.43	0.27201	0.65289	0.92490	
16	504.58	0.0008064	0.040798	73.31	165.62	238.93	73.72	185.80	259.51	0.28157	0.64252	0.92409	
18	537.52	0.0008112	0.038317	76.07	163.92	239.99	76.51	184.08	260.59	0.29111	0.63219	0.92330	
20	572.07	0.0008160	0.036012	78.85	162.19	241.04	79.32	182.33	261.64	0.30062	0.62192	0.92254	
22	608.27	0.0008209	0.033867	81.64	160.45	242.09	82.14	180.55	262.69	0.31012	0.61168	0.92180	
24	646.18	0.0008260	0.031869	84.44	158.68	243.13	84.98	178.74	263.72	0.31959	0.60148	0.92107	
26	685.84	0.0008312	0.030008	87.26	156.89	244.15	87.83	176.90	264.73	0.32905	0.59131	0.92036	
28	727.31	0.0008366	0.028271	90.09	155.08	245.17	90.70	175.03	265.73	0.33849	0.58117	0.91967	
30	770.64	0.0008421	0.026648	92.93	153.24	246.17	93.58	173.13	266.71	0.34792	0.57105	0.91897	
32	815.89	0.0008477	0.025131	95.79	151.37	247.17	96.49	171.19	267.67	0.35734	0.56095	0.91829	
34	863.11	0.0008535	0.023712	98.67	149.48	248.15	99.41	169.21	268.61	0.36675	0.55086	0.91760	
36	912.35	0.0008595	0.022383	101.56	147.55	249.11	102.34	167.19	269.53	0.37615	0.54077	0.91692	
38	963.68	0.0008657	0.021137	104.47	145.60	250.07	105.30	165.13	270.44	0.38554	0.53068	0.91622	
40	1017.1	0.0008720	0.019968	107.39	143.61	251.00	108.28	163.03	271.31	0.39493	0.52059	0.91552	
42	1072.8	0.0008786	0.018870	110.34	141.59	251.92	111.28	160.89	272.17	0.40432	0.51048	0.91480	
44	1130.7	0.0008854	0.017837	113.30	139.53	252.83	114.30	158.70	273.00	0.41371	0.50036	0.91407	

TABL	TABLE A-11													
Saturated refrigerant-134a—Temperature table (Concluded)														
		<i>Specific</i> m³/	Inte	ernal energ kJ/kg	gy,	Enthalpy, kJ/kg				<i>Entropy,</i> kJ/kg·К				
Temp., <i>T°</i> C	Sat. press., <i>P</i> <sub>sat</sub> kPa	Sat. liquid, v <sub>f</sub>	Sat. vapor, v <sub>g</sub>	Sat. liquid, <i>u<sub>f</sub></i>	Evap., <i>u<sub>fg</sub></i>	Sat. vapor, u <sub>g</sub>	Sat. liquid, <i>h<sub>f</sub></i>	Evap., h <sub>fg</sub>	Sat. vapor, <i>h<sub>g</sub></i>	Sat. Iiquid, <i>s<sub>f</sub></i>	Evap., <i>s<sub>fg</sub></i>	Sat. vapor, <i>s<sub>g</sub></i>		
46 48 52 56 60 65 70 75 80 85 90 95	1191.0 1253.6 1386.2 1529.1 1682.8 1891.0 2118.2 2365.8 2635.3 2928.2 3246.9 3594.1 2925.1	0.0008924 0.0008997 0.0009151 0.0009498 0.0009751 0.001037 0.0010373 0.0010774 0.0011273 0.0011938 0.0012945	0.016866 0.015951 0.014276 0.012782 0.011434 0.009959 0.008650 0.007486 0.006439 0.005484 0.004591 0.003713 0.002657	116.28 119.28 125.35 131.52 137.79 145.80 154.03 162.55 171.43 180.81 190.94 202.49	137.43 135.30 130.89 126.29 121.45 115.06 108.17 100.62 92.22 82.64 71.19 56.25 20.72	253.71 254.58 256.24 257.81 259.23 260.86 262.20 263.17 263.66 263.45 262.13 258.73 248.46	117.34 120.41 126.62 132.94 139.38 147.64 156.15 165.01 174.27 184.11 194.82 207.14	156.46 154.17 149.41 144.41 139.09 132.05 124.37 115.87 106.35 95.39 82.22 64.94	273.80 274.57 276.03 277.35 278.47 279.69 280.52 280.88 280.63 279.51 277.04 272.08	0.42311 0.43251 0.45136 0.47028 0.48930 0.51330 0.553763 0.56252 0.58812 0.61487 0.64354 0.67605	0.49020 0.48001 0.45948 0.43870 0.41746 0.36239 0.36239 0.33279 0.30113 0.26632 0.22638 0.17638	0.91331 0.91252 0.91084 0.90898 0.90676 0.90379 0.90002 0.89531 0.88925 0.88120 0.86991 0.85243 0.81202		

Source of Data: Tables A-11 through A-13 are generated using the Engineering Equation Solver (EES) software developed by S. A. Klein and F. L. Alvarado. The routine used in calculations is the R134a, which is based on the fundamental equation of state developed by R. Tillner–Roth and H.D. Baehr, "An International Standard Formulation for the Thermodynamic Properties of 1,1,1,2-Tetrafluoroethane (HFC-134a) for temperatures from 170 K to 455 K and pressures up to 70 MPa," *J. Phys. Chem, Ref. Data*, Vol. 23, No. 5, 1994. The enthalpy and entropy values of saturated liquid are set to zero at -40°C (and -40°F).

# Υ

TABL	TABLE A-12													
Satura	ated refrig	erant-134a-	-Pressure t	able										
		Specific	volume,	Inte	rnal enei	rgy,		Enthalpy			Entropy,			
		m <sup>3</sup> /	/kg		kJ/kg		kJ/kg			kJ/kg·K				
Press.,	Sat.	Sat.	Sat.	Sat.		Sat.	Sat.		Sat.	Sat.		Sat.		
Ρ	temp.,	liquid,	vapor,	liquid,	Evap.,	vapor,	liquid,	Evap.,	vapor,	liquid,	Evap.,	vapor,		
kPa	$T_{sat}$ °C	V <sub>f</sub>	Vg	U <sub>f</sub>	U <sub>fg</sub>	Ug	h <sub>f</sub>	h <sub>fg</sub>	h <sub>g</sub>	Sf	S <sub>fg</sub>	Sg		
60	-36.95	0.0007097	0.31108	3.795	205.34	209.13	3.837	223.96	227.80	0.01633	0.94812	0.96445		
70	-33.87	0.0007143	0.26921	7.672	203.23	210.90	7.722	222.02	229.74	0.03264	0.92783	0.96047		
80	-31.13	0.0007184	0.23749	11.14	201.33	212.48	11.20	220.27	231.47	0.04707	0.91009	0.95716		
90	-28.65	0.0007222	0.21261	14.30	199.60	213.90	14.36	218.67	233.04	0.06003	0.89431	0.95434		
100	-26.37	0.0007258	0.19255	17.19	198.01	215.21	17.27	217.19	234.46	0.07182	0.88008	0.95191		
120	-22.32	0.0007323	0.16216	22.38	195.15	217.53	22.47	214.52	236.99	0.09269	0.85520	0.94789		
140	-18.77	0.0007381	0.14020	26.96	192.60	219.56	27.06	212.13	239.19	0.11080	0.83387	0.94467		
160	-15.60	0.0007435	0.12355	31.06	190.31	221.37	31.18	209.96	241.14	0.12686	0.81517	0.94202		
180	-12.73	0.0007485	0.11049	34.81	188.20	223.01	34.94	207.95	242.90	0.14131	0.79848	0.93979		
200	-10.09	0.0007532	0.099951	38.26	186.25	224.51	38.41	206.09	244.50	0.15449	0.78339	0.93788		
240	-5.38	0.0007618	0.083983	44.46	182.71	227.17	44.64	202.68	247.32	0.17786	0.75689	0.93475		
280	-1.25	0.0007697	0.072434	49.95	179.54	229.49	50.16	199.61	249.77	0.19822	0.73406	0.93228		
320	2.46	0.0007771	0.063681	54.90	176.65	231.55	55.14	196.78	251.93	0.21631	0.71395	0.93026		
360	5.82	0.0007840	0.056809	59.42	173.99	233.41	59.70	194.15	253.86	0.23265	0.69591	0.92856		
400	8.91	0.0007905	0.051266	63.61	171.49	235.10	63.92	191.68	255.61	0.24757	0.67954	0.92711		
450	12.46	0.0007983	0.045677	68.44	168.58	237.03	68.80	188.78	257.58	0.26462	0.66093	0.92555		
500	15./1	0.0008058	0.041168	72.92	165.86	238.77	/3.32	186.04	259.36	0.28021	0.64399	0.92420		
000	18.73	0.0008129	0.037452	77.09	163.29	240.38	//.54	183.44	260.98	0.29460	0.62842	0.92302		
600	21.00	0.0008198	0.034335	81.01	160.84	241.80	81.50	180.95	262.46	0.30799	0.61398	0.92196		
700	24.20	0.0008265	0.031680	04.7Z	156.07	243.23	80.20	176.00	203.82	0.32052	0.60048	0.92100		
700	20.09	0.0008331	0.029392	00.24	150.27	244.01	00.02	174.02	200.00	0.33232	0.56760	0.92012		
800	23.00	0.0008355	0.027598	91.09	152.02	245.70	92.22	171.86	267.24	0.34348	0.57562	0.91950		
850	33.45	0.0008519	0.023043	97.88	152.02	240.02	98.61	169 75	268.36	0.35408	0.55362	0.91779		
900	35.51	0.0008580	0.022703	100.84	148.03	248.88	101.62	167.69	269.31	0.37383	0.53326	0.91709		
950	37.48	0.0008640	0.021456	103.70	146.11	249.82	104.52	165.68	270.20	0.38307	0.53333	0.91641		
1000	39.37	0.0008700	0.020329	106.47	144.24	250.71	107.34	163.70	271.04	0.39196	0.52378	0.91574		
1200	46.29	0.0008935	0.016728	116.72	137.12	253.84	117.79	156.12	273.92	0.42449	0.48870	0.91320		
1400	52.40	0.0009167	0.014119	125.96	130.44	256.40	127.25	148.92	276.17	0.45325	0.45742	0.91067		
1600	57.88	0.0009400	0.012134	134.45	124.05	258.50	135.96	141.96	277.92	0.47921	0.42881	0.90802		
1800	62.87	0.0009639	0.010568	142.36	117.85	260.21	144.09	135.14	279.23	0.50304	0.40213	0.90517		
2000	67.45	0.0009887	0.009297	149.81	111.75	261.56	151.78	128.36	280.15	0.52519	0.37684	0.90204		
2500	77.54	0.0010567	0.006941	167.02	96.47	263.49	169.66	111.18	280.84	0.57542	0.31701	0.89243		
3000	86.16	0.0011410	0.005272	183.09	80.17	263.26	186.51	92.57	279.08	0.62133	0.25759	0.87893		



TABL	E A-13											
Super	heated ref	rigerant-1	34a									
Т	v	и	h	s	v	и	h	s	v	и	h	s
°C	m <sup>3</sup> /kg	kJ/kg	kJ/kg	kJ/kg∙K	m³/kg	kJ/kg	kJ/kg	kJ/kg∙K	m <sup>3</sup> /kg	kJ/kg	kJ/kg	kJ/kg∙K
	P = 0.0	)6 MPa ( <i>T</i>	<sub>sat</sub> = -36.	.95°C)	<i>P</i> = 0.	10 MPa (7	$_{sat} = -26$	.37°C)	$P = 0.14 \text{ MPa} (T_{\text{sat}} = -18.77^{\circ}\text{C})$			
Sat.	0.31108	209.13	227.80	0.9645	0.19255	215.21	234.46	0.9519	0.14020	219.56	239.19	0.9447
-20	0.33608	220.62	240.78	1.0175	0.19841	219.68	239.52	0.9721				
-10	0.35048	227.57	248.60	1.0478	0.20743	226.77	247.51	1.0031	0.14605	225.93	246.37	0.9724
10	0.364/6	234.67	256.56	1.0775	0.21630	233.97	255.60	1.0333	0.15263	233.25	254.61	1.0032
20	0.37893	241.94	204.00	1.1067	0.22506	241.52	203.82	1.0628	0.15908	240.08	202.95	1.0551
30	0.40705	256.97	281.39	1.1637	0.24233	256.46	280.69	1.1204	0.17172	255.95	279.99	1.0913
40	0.42102	264.73	289.99	1.1916	0.25088	264.27	289.36	1.1485	0.17794	263.80	288.72	1.1196
50	0.43495	272.66	298.75	1.2192	0.25937	272.24	298.17	1.1762	0.18412	271.81	297.59	1.1475
60	0.44883	280.75	307.68	1.2464	0.26783	280.36	307.15	1.2036	0.19025	279.97	306.61	1.1750
70	0.46269	289.01	316.77	1.2732	0.27626	288.65	316.28	1.2306	0.19635	288.29	315.78	1.2021
80	0.47651	297.43	326.02	1.2998	0.28465	297.10	325.57	1.2573	0.20242	296.77	325.11	1.2289
100	0.49032	306.02	335.43	1.3261	0.29303	305./1	335.01	1.2836	0.20847	305.40	334.59	1.2554
100	0.50410	514.70	545.01	1.5521	0.50156	514.40	544.01	1.5057	0.21449	514.15	544.22	1.2015
	P=0.	18 MPa (1	$T_{\rm sat} = -12$	2.73°C)	P = 0	.20 MPa (	$T_{\rm sat} = -10$	).09°C)	$P = 0.24 \text{ MPa} (T_{\text{sat}} = -5.38^{\circ}\text{C})$			
Sat.	0.11049	223.01	242.90	0.9398	0.09995	224.51	244.50	0.9379	0.08398	227.17	247.32	0.9348
-10	0.11189	225.04	245.18	0.9485	0.09991	224.57	244.56	0.9381				
0	0.11722	232.49	253.59	0.9799	0.10481	232.11	253.07	0.9699	0.08617	231.30	251.98	0.9520
20	0.12240	240.02	202.00	1.0103	0.10955	239.09	201.00	1.0005	0.09026	239.00	260.00	1.0124
20	0.12740	255.43	270.00	1.0400	0.11418	255 16	278.91	1.0504	0.09423	254.63	209.30	1.0134
40	0.13741	263.33	288.07	1.0976	0.12322	263.09	287.74	1.0882	0.10193	262.61	287.07	1.0718
50	0.14230	271.38	297.00	1.1257	0.12766	271.16	296.70	1.1164	0.10570	270.73	296.09	1.1002
60	0.14715	279.58	306.07	1.1533	0.13206	279.38	305.79	1.1441	0.10942	278.98	305.24	1.1281
70	0.15196	287.93	315.28	1.1806	0.13641	287.75	315.03	1.1714	0.11310	287.38	314.53	1.1555
80	0.15673	296.43	324.65	1.2075	0.14074	296.27	324.41	1.1984	0.11675	295.93	323.95	1.1826
90	0.16149	305.09	334.16	1.2340	0.14504	304.93	333.94	1.2250	0.12038	304.62	333.51	1.2093
100	0.16622	313.90	343.82	1.2603	0.14933	313.75	343.62	1.2513	0.12398	313.46	343.22	1.2356
	P = 0	.28 MPa (	$T_{\rm sat} = -1$	.25°C)	P =	0.32 MPa	$(T_{\rm sat} = 2.4)$	46°C)	P = (	0.40 MPa	$(T_{\rm sat} = 8.9$	1°C)
Sat.	0.07243	229.49	249.77	0.9323	0.06368	231.55	251.93	0.9303	0.051266	235.10	255.61	0.9271
0	0.07282	230.46	250.85	0.9362								
10	0.07646	238.29	259.70	0.9681	0.06609	237.56	258.70	0.9545	0.051506	235.99	256.59	0.9306
20	0.07997	246.15	268.54	0.9987	0.06925	245.51	267.67	0.9856	0.054213	244.19	265.88	0.9628
30	0.08338	254.08	277.42	1.0285	0.07231	253.52	2/6.66	1.0158	0.056/96	252.37	275.09	0.9937
40 50	0.06072	202.12	200.40	1.0577	0.07530	260.83	200.72	1.0452	0.059292	268.92	204.52	1.0237
60	0.09000	278.58	295.40	1 1143	0.07823	209.03	204.07	1 1022	0.064104	200.92	302.98	1.0525
70	0.09644	287.01	314.01	1.1419	0.08395	286.64	313.50	1.1299	0.066443	285.88	312.45	1.1095
80	0.09961	295.59	323.48	1.1690	0.08675	295.24	323.00	1.1572	0.068747	294.54	322.04	1.1370
90	0.10275	304.30	333.07	1.1958	0.08953	303.99	332.64	1.1841	0.071023	303.34	331.75	1.1641
100	0.10587	313.17	342.81	1.2223	0.09229	312.87	342.41	1.2106	0.073274	312.28	341.59	1.1908
110	0.10897	322.18	352.69	1.2484	0.09503	321.91	352.31	1.2368	0.075504	321.35	351.55	1.2172
120	0.11205	331.34	362.72	1.2742	0.09775	331.08	362.36	1.2627	0.077717	330.56	361.65	1.2432
130	0.11512	340.65	372.88	1.2998	0.10045	340.41	372.55	1.2883	0.079913	339.92	371.89	1.2689
140	0.11818	350.11	383.20	1.3251	0.10314	349.88	382.89	1.3136	0.082096	349.42	382.26	1.2943

TABI	TABLE A-13											
Supe	rheated refr	igerant-1	34a ( <i>Coi</i>	ncluded)								
Т	V	и	h	s	v	u	h	s	v	и	h	s
°C	m <sup>3</sup> /kg	kJ/kg	kJ/kg	kJ/kg∙K	m <sup>3</sup> /kg	kJ/kg	kJ/kg	kJ/kg∙K	m <sup>3</sup> /kg	kJ/kg	kJ/kg	kJ/kg∙K
	P = 0.5	50 MPa (7	- <sub>sat</sub> = 15.7	'1°C)	P = 0.	60 MPa (1	$T_{\rm sat} = 21.9$	55°C)	$P = 0.70 \text{ MPa} (T_{\text{sat}} = 26.69^{\circ}\text{C})$			
Sat.	0.041168	238.77	259.36	0.9242	0.034335	241.86	262.46	0.9220	0.029392	244.51	265.08	0.9201
20	0.042115	242.42	263.48	0.9384								
30	0.044338	250.86	273.03	0.9704	0.035984	249.24	270.83	0.9500	0.029966	247.49	268.47	0.9314
40	0.046456	259.27	282.50	1.0011	0.037865	257.88	280.60	0.9817	0.031696	256.41	278.59	0.9642
50	0.048499	267.73	291.98	1.0309	0.039659	266.50	290.30	1.0122	0.033322	265.22	288.54	0.9955
60	0.050485	276.27	301.51	1.0600	0.041389	275.17	300.00	1.0417	0.034875	274.03	298.44	1.0257
70	0.052427	284.91	311.12	1.0884	0.043069	283.91	309.75	1.0706	0.036373	282.88	308.34	1.0550
80	0.054331	293.65	320.82	1.1163	0.044710	292.74	319.57	1.0988	0.037829	291.81	318.29	1.0835
90	0.056205	302.52	330.63	1.1436	0.046318	301.69	329.48	1.1265	0.039250	300.84	328.31	1.1115
100	0.058053	311.52	340.55	1.1706	0.04/900	310.75	339.49	1.1536	0.040642	309.96	338.41	1.1389
110	0.059880	320.65	350.59	1.19/1	0.049458	319.93	349.61	1.1804	0.042010	319.21	348.61	1.1659
120	0.06168/	329.91	360.75	1.2233	0.050997	329.24	359.84	1.2068	0.043358	328.57	358.92	1.1925
140	0.065256	240.05	201 /7	1.2492	0.052519	210.09	200.60	1.2520	0.044000	247.67	270.00	1.2100
140	0.065256	340.00	301.47	1.2747	0.054027	340.20	300.00	1.2000	0.048004	347.07	390 54	1.2445
160	0.068775	368.34	402.73	1.3250	0.057006	367.83	402.03	1.3089	0.048597	367.31	401.32	1.2952
	P = 0.3	80 MPa (7	r <sub>sat</sub> = 31.3	1℃)	<i>P</i> = 0	.90 MPa (	$(T_{sat} = 35)$	.51°C)	$P = 1.00 \text{ MPa} (T_{ext} = 39.37^{\circ}\text{C})$			
Sat.	0.025645	246.82	267.34	0.9185	0.022686	248.82	269.25	0.9169	0.020319	250.71	271.04	0.9157
40	0.027035	254.84	276.46	0.9481	0.023375	253.15	274.19	0.9328	0.020406	251.32	271.73	0.9180
50	0.028547	263.87	286.71	0.9803	0.024809	262.46	284.79	0.9661	0.021796	260.96	282.76	0.9526
60	0.029973	272.85	296.82	1.0111	0.026146	271.62	295.15	0.9977	0.023068	270.33	293.40	0.9851
70	0.031340	281.83	306.90	1.0409	0.027413	280.74	305.41	1.0280	0.024261	279.61	303.87	1.0160
80	0.032659	290.86	316.99	1.0699	0.028630	289.88	315.65	1.0574	0.025398	288.87	314.27	1.0459
90	0.033941	299.97	327.12	1.0982	0.029806	299.08	325.90	1.0861	0.026492	298.17	324.66	1.0749
100	0.035193	309.17	337.32	1.1259	0.030951	308.35	336.21	1.1141	0.027552	307.52	335.08	1.1032
110	0.036420	318.47	347.61	1.1531	0.032068	317.72	346.58	1.1415	0.028584	316.96	345.54	1.1309
120	0.037625	327.89	357.99	1.1798	0.033164	327.19	357.04	1.1684	0.029592	326.49	356.08	1.1580
140	0.038813	337.42	308.47	1.2062	0.034241	330.78	307.09	1.1949	0.030581	330.12	300./0	1.1847
140	0.039985	347.08	379.07	1.2321	0.035302	340.48	3/8.20	1.2211	0.031554	343.87	377.42	1.2110
160	0.041145	366.78	400.61	1 2830	0.037384	366.25	300.01	1 2722	0.032312	365 71	300.24	1 2624
170	0.043427	376.83	411 57	1.3081	0.038408	376.33	410.89	1 2973	0.034392	375.82	410.22	1 2876
180	0.044554	387.01	422.65	1.3328	0.039423	386.54	422.02	1.3221	0.035317	386.06	421.38	1.3125
	P = 1.2	20 MPa (7	- <sub>sat</sub> = 46.2	:9°C)	P = 1	.40 MPa	$(T_{sat} = 52)$	.40°C)	P = 1.6	50 MPa (7	sat = 57.8	38°C)
Sat.	0.016728	253.84	273.92	0.9132	0.014119	256.40	276.17	0.9107	0.012134	258.50	277.92	0.9080
50	0.017201	257.64	278.28	0.9268								
60	0.018404	267.57	289.66	0.9615	0.015005	264.46	285.47	0.9389	0.012372	260.91	280.71	0.9164
70	0.019502	277.23	300.63	0.9939	0.016060	274.62	297.10	0.9733	0.013430	271.78	293.27	0.9536
80	0.020529	286.77	311.40	1.0249	0.017023	284.51	308.34	1.0056	0.014362	282.11	305.09	0.9875
90	0.021506	296.28	322.09	1.0547	0.017923	294.28	319.37	1.0364	0.015215	292.19	316.53	1.0195
100	0.022442	305.81	332.74	1.0836	0.018778	304.01	330.30	1.0661	0.016014	302.16	327.78	1.0501
120	0.023348	325.05	354 12	1.1119	0.019597	313.76	352.00	1.0949	0.016773	322.09	350.93	1.1095
120	0.024228	323.05	364.00	1.1395	0.020368	323.00	363.02	1.1250	0.017500	322.03	361.14	1 1360
140	0.025027	344.63	375 74	1 1031	0.021105	343 34	374 01	1 1773	0.018201	342.02	372 27	1 1633
150	0.026753	354.57	386.68	1.2192	0.022636	353.37	385.07	1.2038	0.019545	352.19	383.46	1.1901
160	0.027566	364.63	397.71	1.2450	0.023355	363.51	396.20	1.2298	0.020194	362.40	394.71	1.2164
170	0.028367	374.80	408.84	1.2704	0.024061	373.75	407.43	1.2554	0.020830	372.71	406.04	1.2422
180	0.029158	385.10	420.09	1.2955	0.024757	384.12	418.78	1.2808	0.021456	383.13	417.46	1.2677

TAB	TABLE A-17												
Ideal	-gas prope	erties of air											
Т	h	-	u		S <sup>o</sup>	Т	h	-	u.		S <sup>o</sup>		
K	kJ/kg	Ρ,	kJ/kg	Vr	kJ/kg∙K	K	kJ/kg	Р,	kJ/kg	Vr	kJ/kg∙K		
200	199.97	0.3363	142.56	1707.0	1.29559	580	586.04	14.38	419.55	115.7	2.37348		
220	209.97	0.3987	149.69	1346.0	1.34444	590 600	596.52 607.02	15.31	427.15	105.8	2.39140		
230	230.02	0.5477	164.00	1205.0	1.43557	610	617.53	17.30	442.42	101.2	2.42644		
240	240.02	0.6355	171.13	1084.0	1.47824	620	628.07	18.36	450.09	96.92	2.44356		
250	250.05	0.7329	178.28	979.0	1.51917	630	638.63	19.84	457.78	92.84	2.46048		
260	260.09	0.8405	185.45	887.8	1.55848	640	649.22	20.64	465.50	88.99	2.47716		
270	270.11	1.0889	192.60	738.0	1.59654	660	670.47	23.13	475.25	81.89	2.49364		
285	285.14	1.1584	203.33	706.1	1.65055	670	681.14	24.46	488.81	78.61	2.52589		
290	290.16	1.2311	206.91	676.1	1.66802	680	691.82	25.85	496.62	75.50	2.54175		
295	295.17	1.3068	210.49	647.9	1.68515	690	702.52	27.29	504.45	72.56	2.55731		
298	298.18	1.3543	212.64	631.9	1.69528	700	713.27	28.80	512.33	69.76 67.07	2.57277		
305	305.22	1.4686	214.07	596.0	1.71865	720	734.82	32.02	528.14	64.53	2.60319		
310	310.24	1.5546	221.25	572.3	1.73498	730	745.62	33.72	536.07	62.13	2.61803		
315	315.27	1.6442	224.85	549.8	1.75106	740	756.44	35.50	544.02	59.82	2.63280		
320	320.29	1.7375	228.42	528.6	1.76690	750	767.29	37.35	551.99	57.63	2.64737		
325	325.31	1.8345	232.02	508.4 189.1	1.78249	760	800.03	39.27	560.01 576.12	55.54 51.64	2.66176		
340	340.42	2.149	242.82	454.1	1.82790	800	821.95	47.75	592.30	48.08	2.71787		
350	350.49	2.379	250.02	422.2	1.85708	820	843.98	52.59	608.59	44.84	2.74504		
360	360.58	2.626	257.24	393.4	1.88543	840	866.08	57.60	624.95	41.85	2.77170		
370	370.67	2.892	264.46	367.2	1.91313	860	888.27	63.09	641.40	39.12	2.79783		
300	200.99	3.170	279.02	343.4 221 5	1.94001	000	910.00	75.20	674 59	24 21	2.82344		
400	400.98	3.806	286.16	301.6	1.99033	900	955.38	82.05	691.28	32.18	2.87324		
410	411.12	4.153	293.43	283.3	2.01699	940	977.92	89.28	708.08	30.22	2.89748		
420	421.26	4.522	300.69	266.6	2.04142	960	1000.55	97.00	725.02	28.40	2.92128		
430	431.43	4.915	307.99	251.1	2.06533	980	1023.25	105.2	741.98	26.73	2.94468		
440	441.61 451.80	5.332	315.30	236.8	2.08870	1000	1046.04	114.0 123.4	758.94	25.17	2.96770		
460	462.02	6.245	329.97	211.4	2.13407	1020	1091.85	133.3	793.36	23.29	3.01260		
470	472.24	6.742	337.32	200.1	2.15604	1060	1114.86	143.9	810.62	21.14	3.03449		
480	482.49	7.268	344.70	189.5	2.17760	1080	1137.89	155.2	827.88	19.98	3.05608		
490	492.74	7.824	352.08	179.7	2.19876	1100	1161.07	167.1	845.33	18.896	3.07732		
500	503.02	8.411 9.031	359.49	162.1	2.21952	1120	1184.28	1/9./	862.79	16.946	3.09825		
520	523.63	9.684	374.36	154.1	2.25997	1140	1230.92	207.2	897.91	16.064	3.13916		
530	533.98	10.37	381.84	146.7	2.27967	1180	1254.34	222.2	915.57	15.241	3.15916		
540	544.35	11.10	389.34	139.7	2.29906	1200	1277.79	238.0	933.33	14.470	3.17888		
550	555.74	11.86	396.86	133.1	2.31809	1220	1301.31	254.7	951.09	13.747	3.19834		
560	565.17	12.66	404.42	127.0	2.33685	1240	1324.93	272.3	968.95	13.069	3.21751		
070	070.00	10.00	111.57	121.2	2.00001								

TABL	TABLE A-17												
Ideal-g	as propertie	es of air (	Concluded)										
Т	h		и		S°	Т	h		и		S°		
К	kJ/kg	Pr	kJ/kg	Vr	kJ/kg∙K	K	kJ/kg	P <sub>r</sub>	kJ/kg	Vr	kJ/kg∙K		
1260	1348.55	290.8	986.90	12.435	3.23638	1600	1757.57	791.2	1298.30	5.804	3.52364		
1280	1372.24	310.4	1004.76	11.835	3.25510	1620	1782.00	834.1	1316.96	5.574	3.53879		
1300	1395.97	330.9	1022.82	11.275	3.27345	1640	1806.46	878.9	1335.72	5.355	3.55381		
1320	1419.76	352.5	1040.88	10.747	3.29160	1660	1830.96	925.6	1354.48	5.147	3.56867		
1340	1443.60	375.3	1058.94	10.247	3.30959	1680	1855.50	974.2	1373.24	4.949	3.58335		
1360	1467.49	399.1	1077.10	9.780	3.32724	1700	1880.1	1025	1392.7	4.761	3.5979		
1380	1491.44	424.2	1095.26	9.337	3.34474	1750	1941.6	1161	1439.8	4.328	3.6336		
1400	1515.42	450.5	1113.52	8.919	3.36200	1800	2003.3	1310	1487.2	3.994	3.6684		
1420	1539.44	478.0	1131.77	8.526	3.37901	1850	2065.3	1475	1534.9	3.601	3.7023		
1440	1563.51	506.9	1150.13	8.153	3.39586	1900	2127.4	1655	1582.6	3.295	3.7354		
1460	1587.63	537.1	1168.49	7.801	3.41247	1950	2189.7	1852	1630.6	3.022	3.7677		
1480	1611.79	568.8	1186.95	7.468	3.42892	2000	2252.1	2068	1678.7	2.776	3.7994		
1500	1635.97	601.9	1205.41	7.152	3.44516	2050	2314.6	2303	1726.8	2.555	3.8303		
1520	1660.23	636.5	1223.87	6.854	3.46120	2100	2377.7	2559	1775.3	2.356	3.8605		
1540	1684.51	672.8	1242.43	6.569	3.47712	2150	2440.3	2837	1823.8	2.175	3.8901		
1560	1708.82	710.5	1260.99	6.301	3.49276	2200	2503.2	3138	1872.4	2.012	3.9191		
1580	1733.17	750.0	1279.65	6.046	3.50829	2250	2566.4	3464	1921.3	1.864	3.9474		

Note: The properties P<sub>r</sub> (relative pressure) and v<sub>r</sub> (relative specific volume) are dimensionless quantities used in the analysis of isentropic processes, and should not be confused with the properties pressure and specific volume.

Source of Data: Kenneth Wark, Thermodynamics, 4th ed. (New York: McGraw-Hill, 1983), pp. 785–86, table A-5. Originally published in J. H. Keenan and J. Kaye, Gas Tables (New York: John Wiley & Sons, 1948).

